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This is a Towler axial plunger oil pump, size A4, which discharges 18.6 cu.ins./sec. up to 5,500 p.s.i. at 1,440 r.p.m. It can be supplied motorised as shown.



2

Two axial pumps can be mounted in tandem, one driven through the other. This example shows a motorised size A4TA4 pump fitted to a tank mounting flange, ready to drop into a tank (which is supplied if required).



3

A vane pump (L series) is available built on to the axial pump. In this example the vane pump is fitted with a relief and unloading valve. From right to left, the combination shown here is A1CL-motor-A4L96. Vane pump discharges up to 1,000 p.s.i. are 21, 34, 61, 96 cu. ins./sec. at 1,500 r.p.m.



4

Towler axial pumps are available with discharges (series A) up to 18.6 cu.ins./sec. at 5,500 p.s.i. at 1,440 r.p.m. or (series XA) 12.4 cu.ins./sec. at 9,000 p.s.i. at 1,440 r.p.m. They are also available for face and foot mounting, packaged in or on a tank; there is full range of valves, and an excellent high pressure system design service is available.

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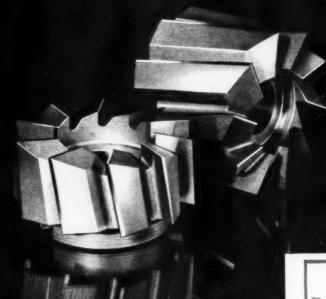
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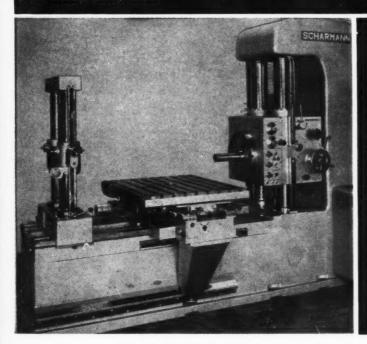
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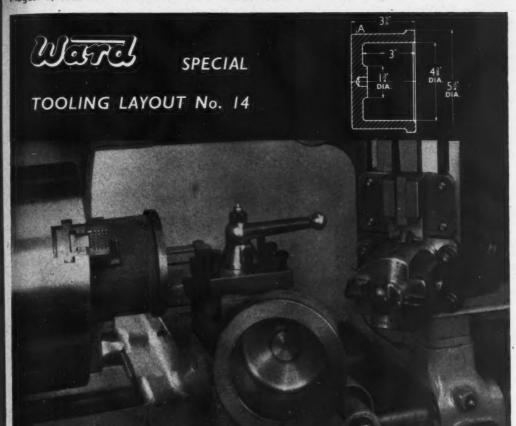




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1							Tool P	osition	Spindle	Max. Cutting Speed		Feed	
	DESCRIPTION OF OPERATION						Hex. Turret	Cross-Slide	Speed R.P.M.	Feet per min.	Metres per min.	Cuts per inch	m/m per rev.
1.	Grip at A					-	_	_	_	_		_	_
2.	Bore 42" dia., face bott	om.	form	end	boss	-	_	_		-	_		-
	and drill &" dia. hole,					-	1	_	(177	278	84-8	76	-334
	Turn flange dia., -		-			-	-	-	119	180	54-7	Hand	Hand
	Chamfer bore & flange	-	-	-		-	_	_	_	_	_		-
	Finish face end -		-	-	-	-	_	Rear	177	278	84-8	Hand	Hand
3.	Remove from chuck	-	-	-	-	-	-	-	-	-	-	-	

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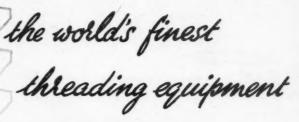
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(seen on machine above)

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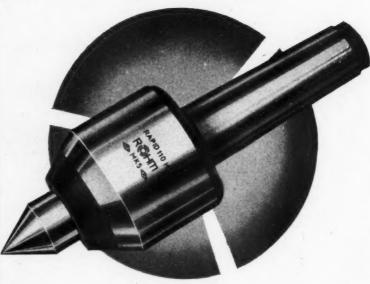


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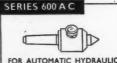




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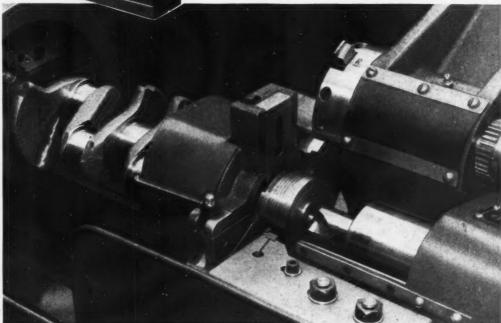
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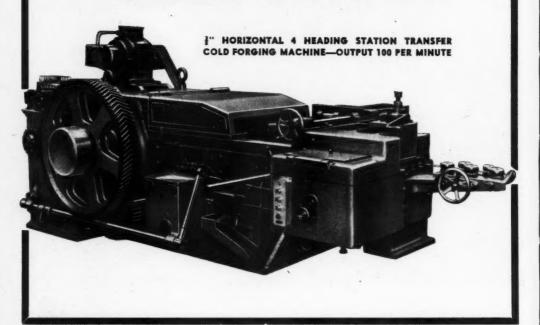
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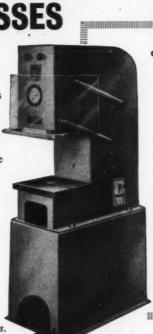
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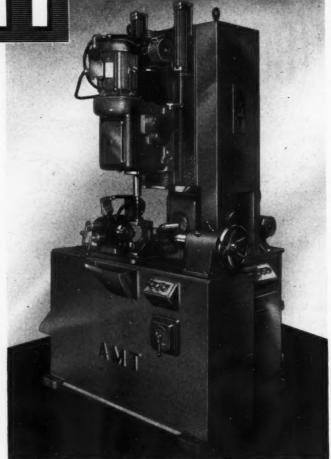
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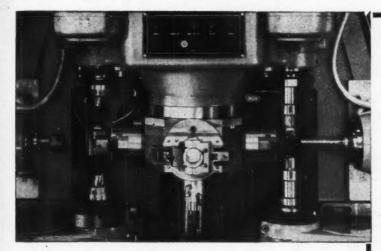
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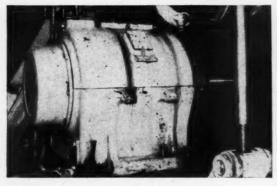
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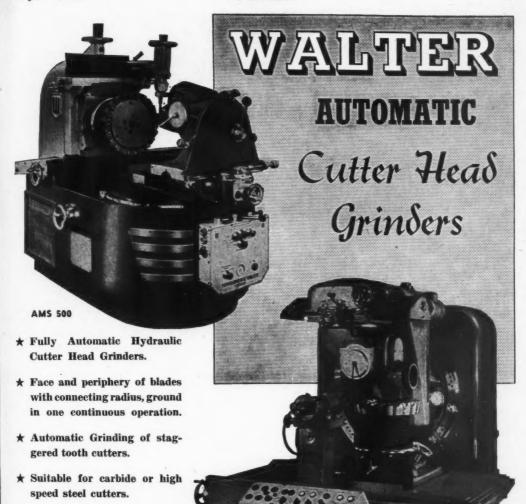
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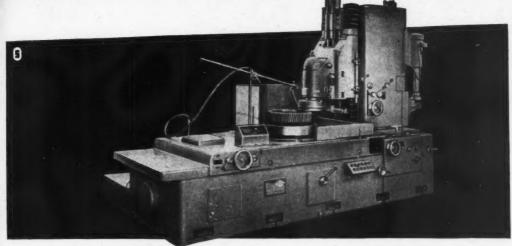
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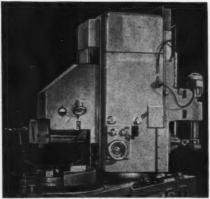


Fig. 2 Surface grinding head with periphery grinding wheel

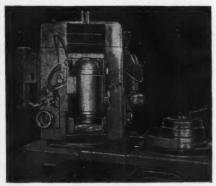


Fig. 3 Model "RFBR" with 3 wheelheads

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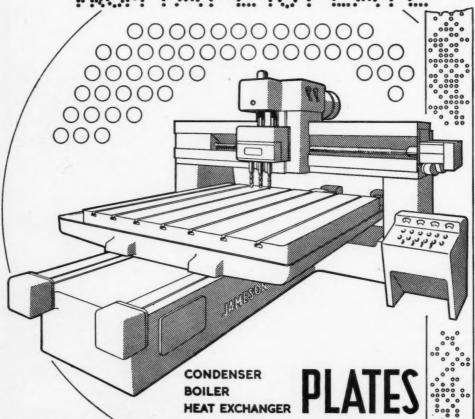
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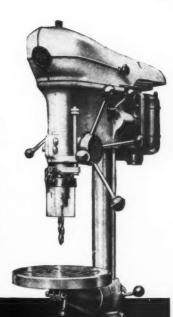
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Sales Office: WARTON ROAD, STRATFORD, LONDON, E.15. Telephone: MARyland 6611



O & S Straightening Presses, made in 5 sizes with capacities ranging from 4 to 60 tons pressure, have for many years been the first choice of engineering firms throughout the world, including most of the leading motor manufacturers. For speed, accuracy and ease of operation, O & S Straightening Presses are in a class of their own.



In the Leicester works of Frederick Parker Ltd., O & S Straightening Presses are in daily service ensuring that steel shafts are perfectly straight and true.



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The O & S Range also includes:

SS & SC lathes from 10½ in. to 24 in. capacity; surfacing and boring lathes up to 96 in. swing; break lathes; railway carriage and wagon wheel lathes; axle journal turning and burnishing lathes; straightening presses.

This lathe will swing up to 6 ft. over the saddle and is specially designed for Turning Drums, Rollers, etc. It is easy to handle, economical in operation and competitively priced. The Big Swing also makes this an ideal machine for general maintenance work.

The 0 & S Big Swing Lathe incorporates all these features:

- Up to 6 ft. swing over saddle
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- 12 spindle speeds
- Large hollow spindle
- Spindle bearings PB or Taper Roller
- 32 enclosed change feed and screw-cutting box
- Long lead cutting gear
- Quick power motion to saddle
- Power feed to compound top slide if required
- Power feed to loose headstock if required
- 30 or 35 H.P. motor drive



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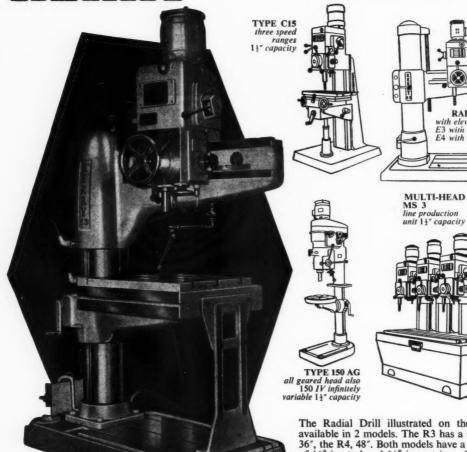


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RADIAL with elevating arm E3 with 46" swing E4 with 58" swing

RANGE OF

DRILLING MACHINES



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The Radial Drill illustrated on the left is available in 2 models. The R3 has a swing of 36", the R4, 48". Both models have a capacity of 1½" in steel and 1½" in cast iron, 9 spindle speeds ranging from 90 to 1120 r.p.m., quick hand traverse, fine hand feed and three rates of power feed. The Kerry range of drilling machines includes bench, pillar and line production models with drilling capacities from ½" to 1½".

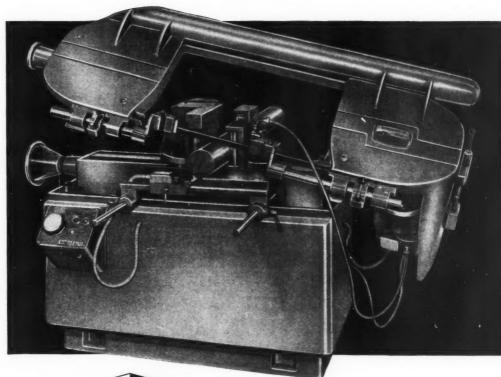


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Broadway QSII





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For higher production

Infinitely variable cutting speeds, accurate blade guidance, faster cutting times, power lifting and lowering of sawframe, simplicity of operation and of blade changing mean higher production than with any comparable saw. The completely automatic cutting cycle facilitates repetition work.

the British made Bandsaw that is in the world's top class

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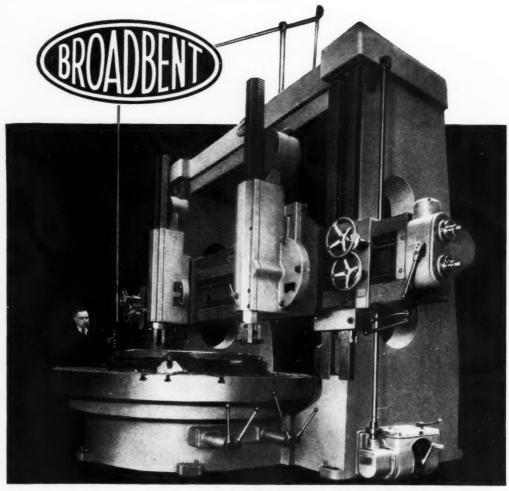
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3611 QS11



HEAVY DUTY Vertical BORING & TURNING MILLS

with 5, 6, 8 or 10 ft diameter work tables

These incomparable machines are massively constructed for years of hard service. Accuracy and dependability are of the high order that industry has learned to expect of Broadbent Machine Tools. Notable features of these Boring and Turning Mills include twelve changes of speed and six changes of feed, controllable from either side of the machine; spiral bevel and spur reduction gears driving the work table; pendant control of rams and cross slides; and rapid power traverse with independent control of the two heads.

Please write for fully illustrated brochure.



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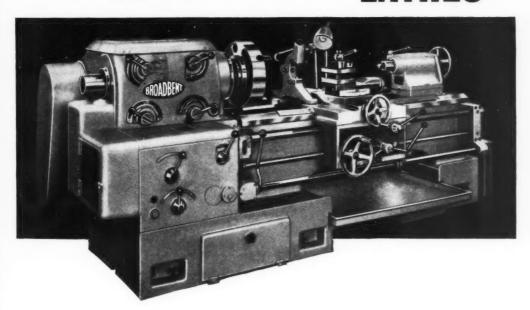


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MORE output per man-hour with

Good men plus good tools equal good output. Every Broadbent lathe incorporates almost a century of machine tool building. Manufacturers know that for versatility, accuracy and reliability there is nothing quite as good as a Broadbent Machine Tool.





This 18/22" Swing Heavy Duty Centre Lathe of modern design is a typical example of the Broadbent range. It has a 15 h.p. drive motor and spindle speeds up to 1,000 r.p.m.

The Broadbent range of Machine Tools includes Surfacing and Screw-cutting Lathes from 17" to 72" swing, Surfacing and Boring Lathes, Break Lathes, Crankshaft Lathes and vertical Turning and Boring Mills with 5', 6', 8' or 10' capacity.



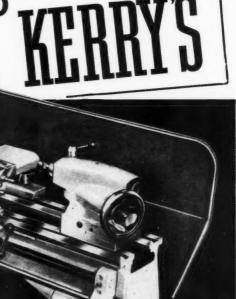
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- * TYPE LOO PRECISION TAPERED SPINDLE NOSE
- ★ FEED BOX GIVES 62 PITCHES AND 7 FEEDS FROM ·0004 in.-·024 in.
- * CAMLOCK TAILSTOCK
- * BEDWAYS AND SLIDES
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- * HARDENED BEDWAYS OPTIONAL EXTRA

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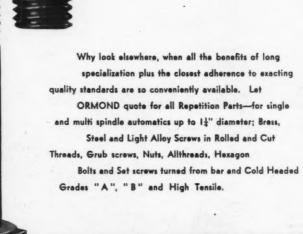








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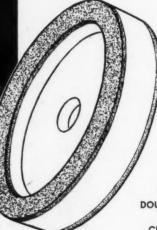
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Specially developed for off-hand grinding of tungsten carbide tipped tools, the Diagrit ES Metal bonded plain cup wheel offers the extra cutting speed and life demanded by the competitive producer. A full range of shapes and sizes in various diamond grades is available. Please complete and post coupon below

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Illustration shows the off-hand lapping of heavy section carbide tipped tools at TILLING-STEVENS LTD., MAIDSTONE.



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22in. and 25in. Swing

Centre Lathes

25in. Swing

Surfacing and **Boring Lathe**

18 Spindle Speeds in alternative ranges up to 1,000 down to 11 r.p.m.

54 Change T.E. Feed Gearbox

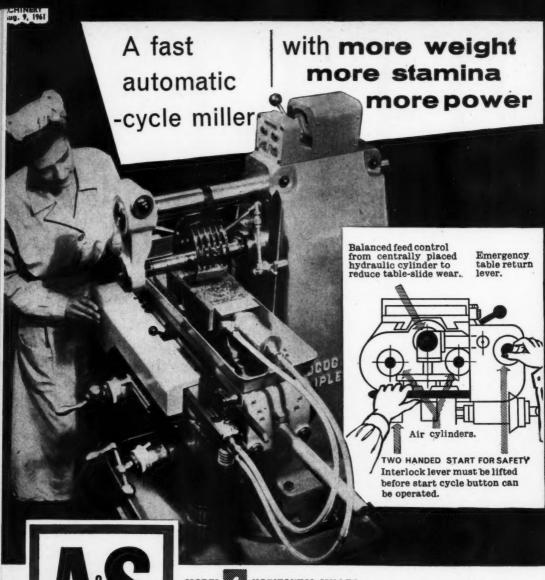
Comprehensive Range Optional Equipment

Centre Lathes from 17in. (430 mm) to 42in. (1065 mm) Swing.

Surfacing and Boring Lathes of 17in. (430 mm) and 25in. (635 mm) Swing

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If you would like to know more about the advantages of the V10B-Sykomatic range, write for a copy of brochure P18/60.

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Great rigidity from box section table mounted directly on bed, with vertical arbor movement by elevating spindle column sliding in vee way at rear of machine, and transverse cutter adjustment by axial movement of arbor. Independent table motions from separate motors give fast traverse and feed for climb milling in both directions, also pendulum milling. Safeguards on table motion trip feed motors in the event of overload.

Table working surface: 50" x 10½".

Spindle centre to table:
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fully automatic table cycle

Spindle speeds from 25 to 880 r.p.m.

30 rates of feed — ½" to 20" per min.

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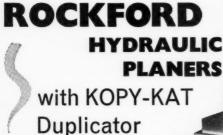
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36", 48", 60" and 72" machines with 24" or 32" x 30" capacity. Infinitely variable cutting speeds up to 110 ft./min.



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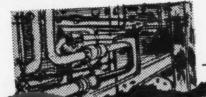


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DENISON VALVES



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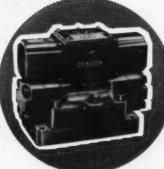
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- Threaded bodies with BSP parallel threads.
- Subplate mounting type complete with subplates.
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- Fast action eliminating over-pressures and pressure drops.
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Relief Valve RV-061303A. Weight 10.5 lb. Cop 16.7 g.p.m.

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OPERATED 1 and 1 4-WAY
VALVES WITH:—

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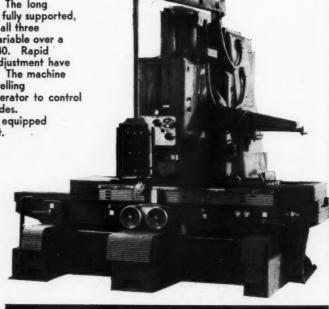
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The guidance of the cross slide on the bed has been designed having three slideways. The long cross slide ensures that the table is fully supported, even in its extreme positions. For all three movements, the feed is infinitely variable over a PIV-gearing in the range from 1:40. Rapid traverse, fine traverse and hand adjustment have been provided for all movements. The machine is centrally controlled from a swivelling pendant station, to enable the operator to control the machine practically from all sides. For profiling the machine can be equipped with automatic copying equipment.

SPECIAL OPTIONAL **EQUIPMENT**

- Optical measuring device for the longitudinal movement of the
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- Climb milling equipment for the longitudinal movement of the table
- Spindle head to swivel mechanically to either side by 45°.
- · Copying equipment with electric tracer control in three dimensions with automatically controlled rapid feeds.
- Automatic retraction of cutter and approach.
- Arrangement of the machine for a programme using feed, rapid traverse and fine traverse in three directions.

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CAPACITY	VF4	VF5	VF6
Working surface of table	63" x 19½" 63" 25"	71" x 25" 71" 274"	781" x 311" 821" 351"
Vertical power movement of spindle head	18‡"	241"	294"
Distance from table to spindle nose Range of speeds Spindle speeds Milling spindle motor	25;" 0-23;" 16-800 r.p.m. 18 18 h.p.	28½" 0-29½" 12.5-630 r.p.m. 18 25 h.p.	37½" 0-37½" 10-500 r.p.m. 18 35 h.p.



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And at Kingsbury (Nr. Tamworth). Manchester, Glasgow, Swansea.

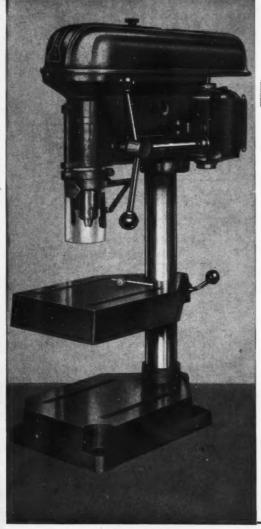
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INCOMPARABLE

IN PRICE & QUALITY

- Weight 154 lbs. 70 kgs.
- Five Spindle Speeds
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- Quill Diameter 2": 50.8 mm
- Robust Spindle and Quill Assembly with splined spindle and driving sleeve
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Supplied complete with 0-lin. Chuck, 3 phase motor, rotary on/off starter. Pedestal model £2.15.0 Extra. Single phase electrics £2.10.0 Extra.

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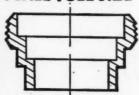
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Operation I Loading 6 secs Machining 28 secs Material—BRASS (Billet)

SCALE FULL SIZE



Operation 2
Loading 6 secs
Machining 43 secs
Material—BRASS
pre-machined blank
from Op. I,





- Work head spindle can automatically operate at high or low speeds according to preselected cutting speeds.
- Camshaft driven from main spindle.
- Cam accelerator reduces machining cycle time.
- Air-operated chucking
- Spindle positioning device for irregular shaped components.
- Easy loading of components into chucks.
- Write for full data.



Illustration shows tailstock which is one of the many optional features available.

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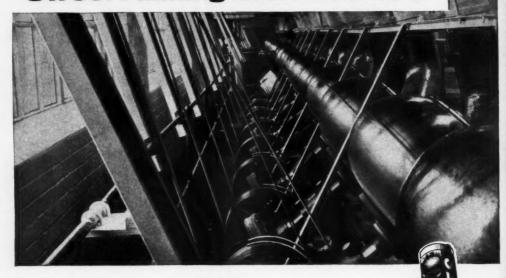
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The sugar panning process shown above demands belting capable of continuous running at carefully maintained speeds for long periods. Turners flat transmission belting is used for this and many other exacting tasks by Rowntree & Co. Ltd. at York. Ensure smooth sweet running on all your drives by using Turners belting.

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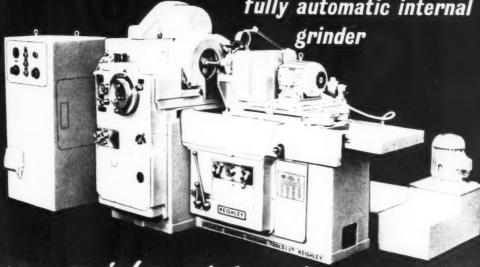
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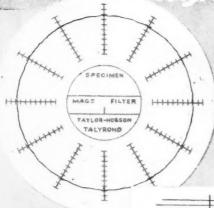


KEIGHLEY AK

fully automatic internal



quicker set-ups



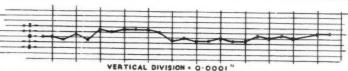
Graph shows accuracy within 0.0002" achieved in production of a batch of components with 1 H " dia. × 1" bore. Production rate-100/hour floor to floor, stock removal -0.008".

> Roundness recorded by TALYRONDwithin 0.00004".

Precision built to exceptionally robust proportions, sperated by single lever control after initial setting up, and arranged for both gauge and diamend sizing to ensure maximum utilisation, the fully automatic AK is unsurpassed for accuracy, component finish and fast cycles in grinding holes from 1" to 6" diameter with a maximum depth of 6", and for taper bores up to 60° included angle.

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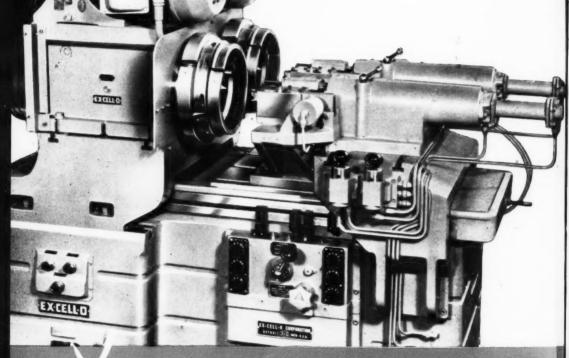
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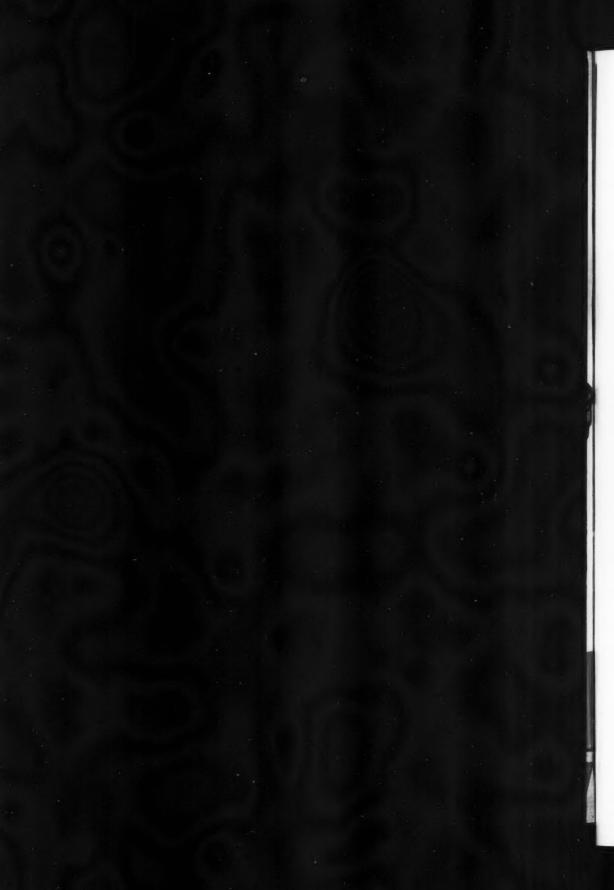
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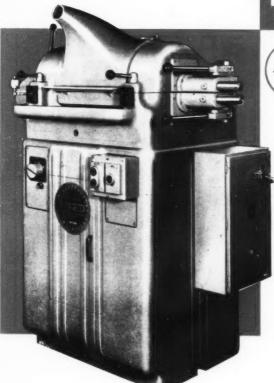
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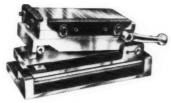


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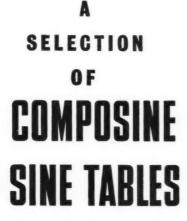
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"WRIGHT" TABLE SURFACE GRINDERS

Wheel diameters from Eight to Twenty Inches



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Eight Model 55/20 machines are now in use in REPAIR and MAIN-TENANCE WORKSHOPS of the Union of South Africa Railways.

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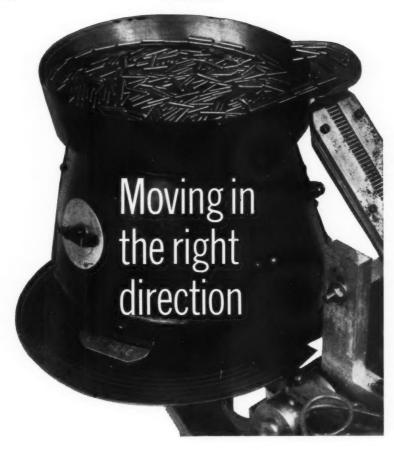
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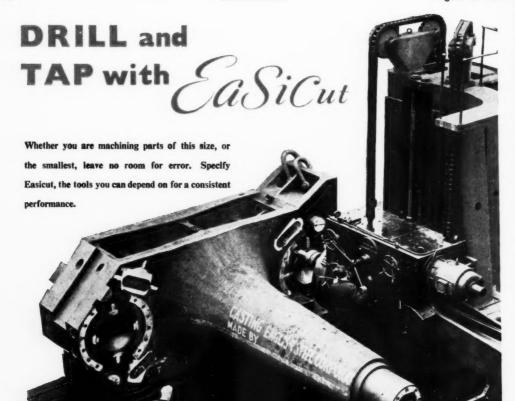
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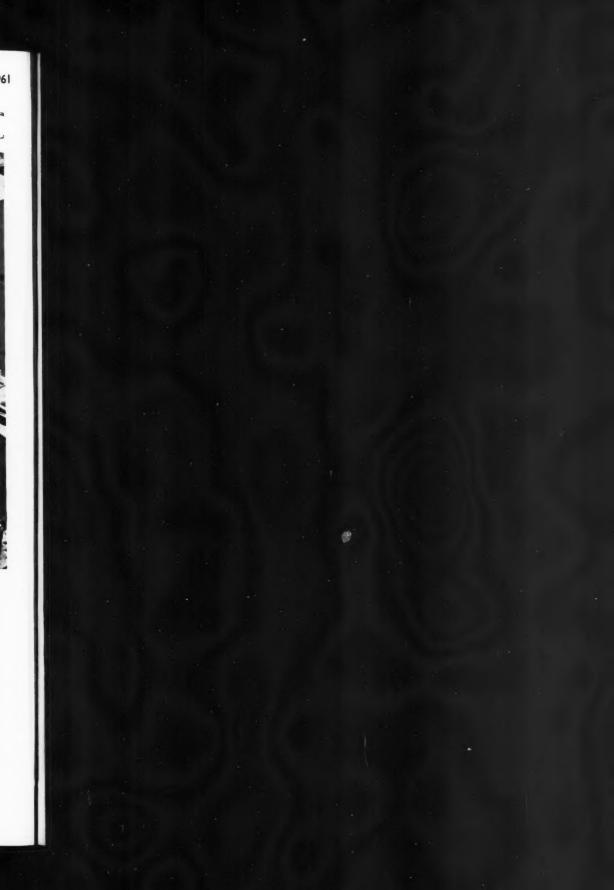
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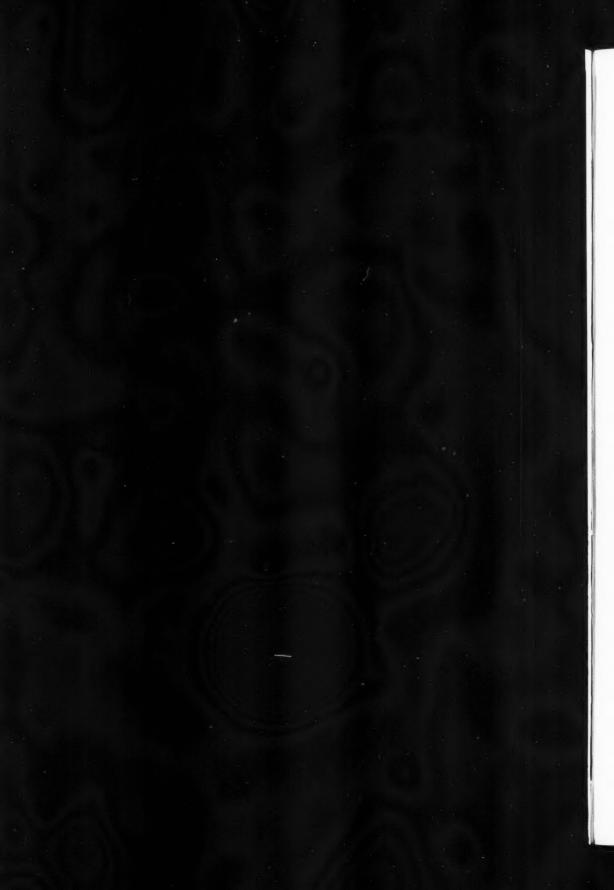
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A wholly owned subsidiary of English Steel Corporation Ltd., Sheffield







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enabling two parallel faces, square and hexagonal shapes to be economically produced as well as slotting, chamfering and drilling operations to be performed at the same time.

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hexagon across flats 0.118-1.417 in. square across flats 0.118-0.944 in. maximum turning length 1.574 in.

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Across flats = 1.023 in. Time per piece... 20 seconds





Across flats = 0.944 in.
Material: Mild steel, approx. 130 lbs/sq. in.
Time per piece... 8 seconds





Across flats = 0.748 in.
Material: Mild steel,
Time per piece... 15 seconds





Length = 0.314 in.
Material: Heat treated steel (CK-45),
approx. 200 lbs/sq. in.
Time per piece... 15 seconds







Across flats = 0.944 in.
Material: Steel (C-35)
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HAHN & KOLB (GREAT BRITAIN) LTD. 243-245 HORN LANE, ACTON, LONDON W 3

EASIER THAN EVER TO OPERATE!

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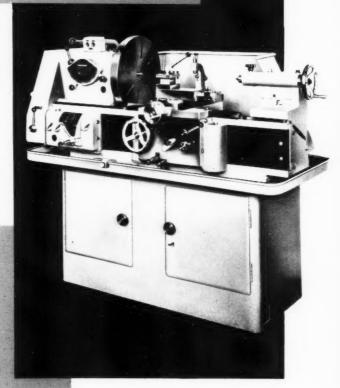
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The WILLSON Inclined Bed Centre Lathe Mark I, represents a unique combination of time-proven design principles, modern refinements, and striking new advances in machine tool technology. Taper roller bearings, totally enclosed motor, extreme rigidity with clean chip flow lines; these will be found on WILLSON Lathes, and in addition are to be found such striking features as the fully protected double inverted wee bed, inclined to admit a full 17-jin. dis. swing by 75 swing without gap and shed swarf; complete enclosure of screw and shaft; isolation of motor upon opening change wheel guard or locking compartment door, etc.

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For accuracy and high surface finish



The Snow Type OS36/18 machine illustrated is installed at B.I.P. Tools Ltd., Birmingham. Its inherent characteristics of robust and rigid construction, powerful wheelhead motor, etc., ensure the production of flat surfaces to close tolerances and high finish so essential in the manufacture of tools for the plastics industry for which B.I.P. Tools Ltd. have established a high reputation.

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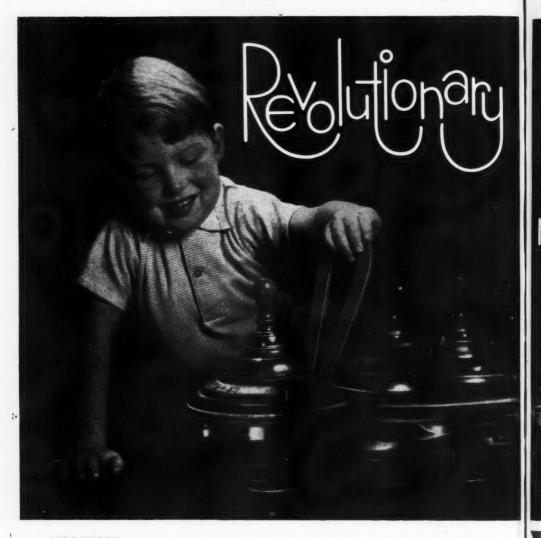
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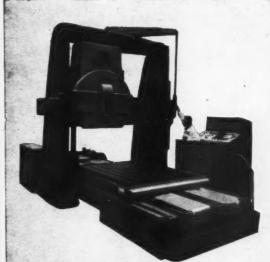


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(Photograph produced by courtesy of James Archdale & Co. Ltd., Worcester)



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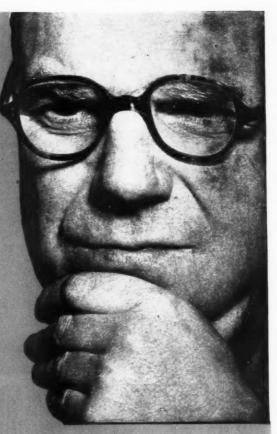
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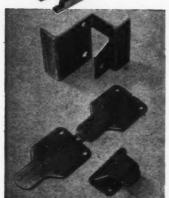


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For forming heavy gauge parts from strip up to 3 inches wide and 12 inches developed length.





Designed with the die space 31 inches long and accommodating three individually operated diesets, if required, each 10 inches long, the Heenan S.3 Mutitiorm is particularly suitable for the automatic forming of parts requiring substantial presswork, such as piercing, stamping, coining, blanking, embossing and trimming, using progression tooling. Press rams can be operated from front or rear, with 30 tons loading to each ram.

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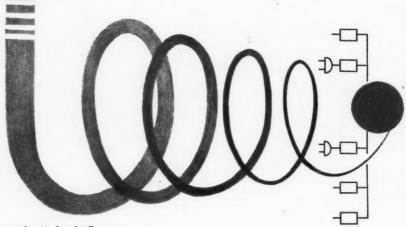


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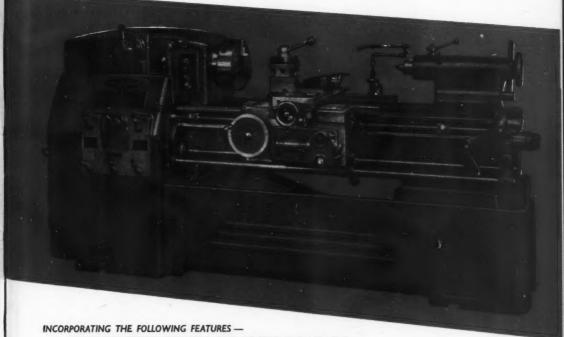
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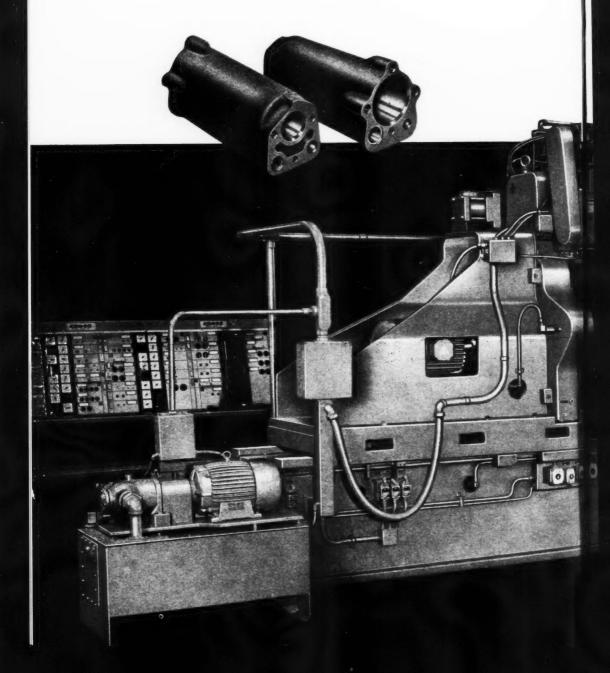
HARLOW 2351

SACHINE TOOL CO.LTD.

CAMBRIDGE ROAD, HARLOW, ESSEX

New Cross Trunnion Machine with Greater Flexibility

Processes remote accessory cylinders of different designs and different materials







Another Automation First by Cross

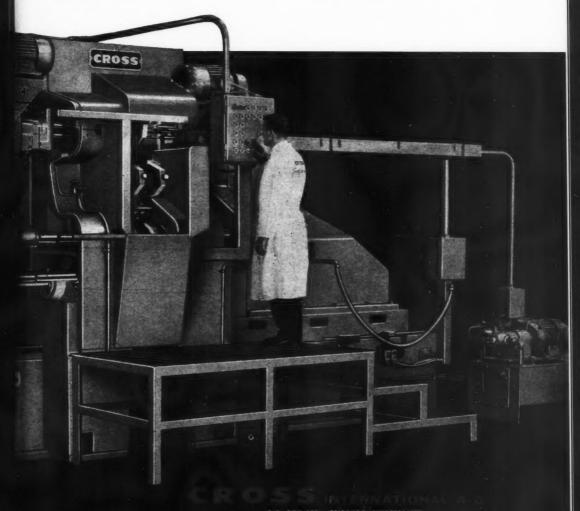
Recent developments by Cross have resulted in trunnion machines that perform a variety of operations on families of parts with improved accuracy and at a higher rate of production than previous equipment.

A typical application of the new design concept is the processing of remote accessory cylinders which vary in both size and material. Different lengths are handled by changing a few tools, replacing some fixture details and adjusting the feed strokes. Both nodular and grey iron castings are processed by changing the speeds and feeds.

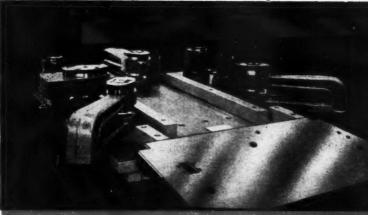
Similar operations such as rough, semi-finish and finish boring; drilling; counterboring and chamfering are completed by spindles in the two main heads. Dissimilar work such as tapping, facing and grooving are done by four auxiliary heads.

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For Milling Machines

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has been specially designed as a heavy duty attachment and makes use of the spindle of an existing Vertical Milling Machine, thus the full power and vertical traverse of the spindle head is available. Built in two sizes, the FRV. attachment is to be regarded as more permanent than the model FR.



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Suitable for fitting to an existing Plain or Universal Horizontal Milling Machine. This attachment has its own motor-driven eight-speed spindle with rise and fall quill controlled by the Hydraulic Tracer. This model is available in three sizes.

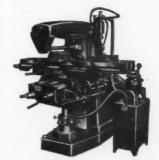


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is supplied in two sizes for Horizontal Milling Machine sizes 1 & and 3 & 4 respectively. The attachment is applied to the vertical traverse of the knee on the front column of the machine which is controlled by the hydraulic tracer mounted above the table.

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Specification

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Bore of spindle			2±in
			A.S.A
Max. swing over be	ed		151in
Max. swing over sa	ddle		93in
Max. length turned			27-in
Hydraulc traverse slide	of cop	ying	4in
Hydraulic feed of	of tails	tock	
spindle			43in
Number of feed	rates	to	
copying slide			4
Max. tool pressure		1,3	300 lbs
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POINT FEATURES INCLUDE

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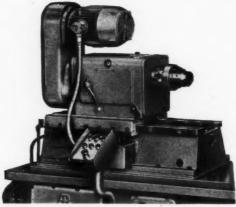
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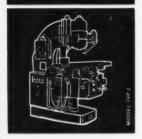












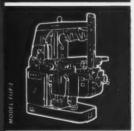


The SAIMP range of fine milling machines

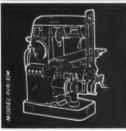
There's a model to suit your needs in this fine range of proven millers - built to the finest limits and beautifully finished. From Italy's leading machine tool factory. Write now for prices and delivery . . .













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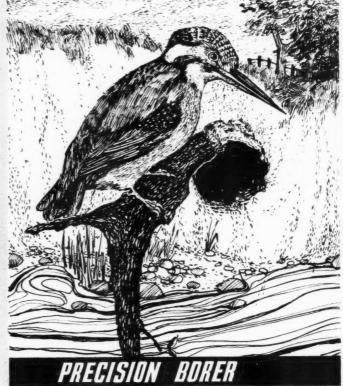
The Kingfisher (Alcedo ispida) nests at the end of a narrow tunnel which it burrows into the bank of a stream, river, pond or lake. The burrow slopes gently upwards for many feet and once constructed is used for many years. In strange contrast to the brilliant plumage of the bird, its burrow is usually in a foul condition being littered with fish-bones and other refuse.

The
Alcedo Ispida
is
Efficient
But hardly a

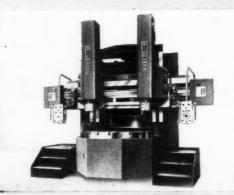
Illustrated right is a
RICHARDS VERTICAL
BORING MILL, supplied in
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from 5ft. to 12ft., with or
without side-head.

RICHARDS

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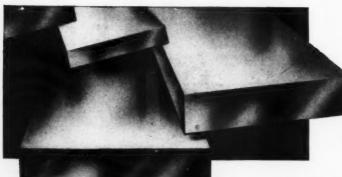


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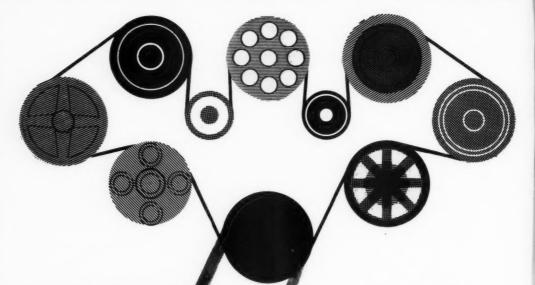
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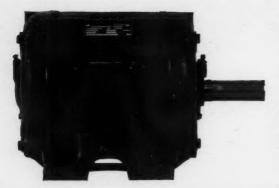
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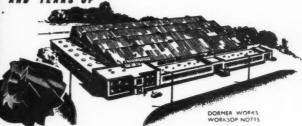
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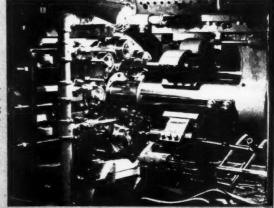
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Editorial

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Abstracts of Principal Articles

Making Petrol Dispensing Pumps .. P. 292

In this article, which is the second in a series concerned with the production of petrol dispensing pumps at the Crayford works of Vickers Armstrongs (Engineers), Ltd., reference is first made to operations on cast-iron air separator housings. An Archdale radial drilling machine is equipped with a special fixture, incorporating five Par-A-Matic pneumatic drills, whereby ten holes are drilled in a flange while other holes are being drilled, spotfaced and tapped, with the main machine spindle. Air for the drills is delivered by way of a supply trolley. Main pump bodies are milled on a Cincinnati duplex machine, six at a time, and the company has built a fixture with air-hydraulic clamping arrangements. Slots are milled in four cast-iron rotor bodies simultaneously, using an indexing fixture and carbide-tipped cutters. A fixture with special support arrangements is used to hold a light alloy casing while the end flanges are milled on an Archdale duplex machine. (MACHINERY, 99—9/8/61.)

Standardization of Machine Tools in East Germany P. 300

This article is concerned with certain aspects of the work of the East German Institute of Machine Tool Engineering, particularly in connection with the introduction of a system of unit construction. Among machine tools to which this principle has so far been applied are lathes, bevel gear generating machines gear shapers, plano-milling machines and planers, and vertical honing machines. Other work undertaken by the institute has included the development, in collaboration with certain machine tool factories, of unit heads suitable for such operations as drilling, tapping, boring, milling and grinding. In-line and rotary transfer machines, also multi-way drilling machines, can be made up from the range of units available, which includes beds, columns, tables, and slides in a number of sizes. Attention has also been paid to the development of tools for performing multiple operations. An example of such tools is a combination roughing and finishing drill fitted with a single reaming blade of tungsten carbide. (MACHINERY, 99—9/8/61.)

Automatic Detection of Broken Tools P. 318

The automatic detection of broken tools is essential in connection with high-production installations, such as transfer machines and link-lines, if timeconsuming and costly interruptions are to be avoided. One method of detection described in this article involves the use of a photo-electric cell and a number of transmitters for monitoring a multi-spindle drilling machine. With another arrangement, the electrical inductance of tools is measured, and if a tool is broken the consequent reduction in inductance is utilized to stop the cycle. (MACHINERY, 99—9/8/61.)

Diaphragm Chucking P. 320

Increasing use is being made in production engineering of diaphragm-type chucks of various designs, and after discussing the principle of operation of such equipment this article describes some typical applications. For holding external spur gears, one type of chuck is provided with interchangeable parts to accommodate workpieces of different sizes, and incorporates ball-ended pegs which engage with the gear teeth for clamping and locating. Another type of chuck is employed to hold internal gears during tooth-cutting, and is designed to resist the high torque loads associated with this operation. (MACHINERY, 99—9/8/61.)

A Quick-acting Centrifugal Governor P. 324

It was required to control the speed of a steam turbine installed in a chemical plant, and the use of a conventional governor was not permissible since a virtually instantaneous response to the critical speed was essential. The governor which was designed for this duty, and is described in this article, is unconventional and incorporates weighted arms which are pivoted about an axis at right-angles to that of the rotation of the governor. The weights are held in a predetermined position by means of a special C-spring, and when the speed of rotation reaches a certain value, the centrifugal force is greater than that exerted by the spring, and the weighted arms change positions very rapidly. This movement is employed to actuate a speed control in a conventional manner. As the rotational speed falls, the C-spring reasserts itself, and the weighted arms change position rapidly once more. (MACHINERY, 99—9/8/61.)

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Producing gas turbine components—Planning for the A.E.I. Numeritrol numerical control system—The activities of Paterex, Ltd.

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EDITORIAL

Overseas Trade in Metal Products

The lack of balance between United Kingdom exports-visible and invisible-and imports continues to cause anxiety, and it is evident that still greater efforts must be made to expand sales in To this end, we must conoverseas markets. centrate even more on achieving higher productivity and improved product quality, to enable us to compete more effectively, and particular attention must be paid to the reduction of delivery periods quoted, and the maintenance of delivery promises. There are, of course, many other factors which influence sales abroad, and the nature of the services offered for repair and replacement of parts can be of particular importance. Numerous British companies have achieved outstanding successes in the export field during the post-war years, sometimes on account of the special merits of the products which they have had to offer, and sometimes because the managements have shown the necessary determination to take advantage of the opportunities afforded.

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One noteworthy aspect of the trade returns during recent years has been the substantial growth in the value of exports of some of the principal metal products, which have accounted for an increasingly large proportion of the total, and it appears that future overall expansion can best be promoted by concentrating on these products more and more. Of particular significance are the results that have been obtained "machinery other than under the heading electric", which necessarily covers a very wide range. In 1956, the value of such exports amounted to £503.6 million out of a total of £3,172 million, so that they accounted for 15.9 per cent of all exports of produce and manufactures. For the first half of this year, exports of "machinery other than electric" were valued at £419 million, which represented 22.4 per cent of the export total of £1,871.5 million.

The next most important group of exports is "road vehicles and aircraft", which reached a value of £372.5 million in 1956 or 11.7 per cent of the overall figure for the year. During the first six months of this year there was a sharp drop in exports under this heading, in comparison with the results achieved in the corresponding period of 1960, mainly on account of the much smaller number of cars consigned to the United States (9,428 as against 103,329). Even so, the value of road vehicle and aircraft exports for the

past six months was £232.8 million, so that they provided 12.4 per cent of all exports, by value.

It is interesting to examine the situation from another standpoint. If the values for "machinery" and "vehicles" are deducted, it is found that the totals for all other exports were £2,296 million in 1956, and £1,219·6 million in the first half of this year, representing an annual rate of £2,439 million. In other words, exports, apart from those in the two selected groups, increased by only 6·2 per cent as between 1956 and the first half of 1961. During the same period, despite the recent setback, exports of "road vehicles and aircraft" rose by 25 per cent, and exports of "machinery other than electric" by no less than 66·4 per cent.

Should these trends continue, then by 1966 the value of "other" exports will have increased to £2,590 million, the value of "road vehicle and aircraft" exports to £582 million, and the value of "machinery other than electric" exports to £1,394 million. By 1971, moreover, the corresponding figures will be £2,750.6 million, £727.5 million, and £2,319.6 million. In other words, the two groups together will account for considerably more than half of all exports.

Other groups of exports of metals and metal goods which showed more than average increases during the period from 1956 to the first half of this year are "iron and steel" and "electric machinery, apparatus and appliances." For the former, the values for 1956 and for the first six months of 1961 were £173·3 million and £113·7 million (annual rate of £227·4 million), and for the latter, £217·3 million and £135 million (annual rate £270 million).

For purposes of comparison it may be noted that imports of "machinery other than electric" rose from £110.5 million in 1956 to £126.6 million (annual rate £253.2 million) in the first six months of this year, imports of "electric machinery, apparatus and appliances" from £23.7 million to £30.4 million (annual rate £60.8 million), and imports of "road vehicles and aircraft" from £23.5 million to £19.6 million (annual rate £39.2 million), whereas imports of "iron and steel" fell from £105.6 million to £25.9 million (annual rate £51.8 million).

So far, the very substantial achievements of the makers of machinery, road vehicles and aircraft (Continued on page 336)

Making Petrol Dispensing Pumps

Methods and Equipment Employed by Vickers Armstrongs (Engineers), Ltd.

By P. A. SIDDERS, Chief Associate Editor

In an earlier article* reference was made to the manufacture of petrol dispensing pumps by Vickers Armstrongs (Engineers), Ltd., Crayford, Kent, under an arrangement with the Gilbert & Barker Mfg. Co., Springfield, U.S.A. Machining of metering pump bodies was described, also the production of brass cylinder liners, which are pressed into the bodies on a special air-operated machine built by the company. Machining operations on some other petrol pump components are here considered.

Each pump incorporates a cast-iron component, known as an air separator body. One of these castings is seen at the upper left in Fig. 1, and it will be observed that it is of bell shape, with external strengthening ribs and a flange at the open end. There is a large facing and a smaller boss at one side, and a second small boss at 180 deg. to

Castings are faced and bored on a Ward No. 8 turret lathe, and a component after the completion of this stage is seen at the upper right in Fig. 1. From the Ward lathe, the workpieces are passed to an Archdale radial drilling machine, and a casting in the condition in which it leaves this machine is seen in the centre of the illustration. The set-up on the Archdale machine provides for boring a cored hole A in the large facing, machining a concentric spot-face B, of 3-in. diameter, and producing a chamfer at the open end of the hole, with a combination tool; tapping the bored hole 2% in. diameter by 16 t.p.i. Whitworth form; drilling and tapping the two smaller bosses %-in. B.S.P., as seen at C; drilling a 1/4-in. diameter hole D through the metal at the bottom of one of the smaller tapped holes; and drilling ten holes # in. diameter in the flange. Fig. 2 is a general view of the Archdale machine, set-up for these operations.

The Archdale machine has a heavy-duty rightangle support mounted on the baseplate, and to the upper face of this support is secured a fixture built by the company. Constructed by welding from steel plate, the fixture has a stirrup-shaped worksupport, as indicated at A in the close-up view, Fig. 3. The work-support is free to rotate, on a horizontal axis, between the main frame of the fixture, and the support bracket B at the opposite end of the base. Holes in the circular end-plate of the work-support are engaged by the hand-operated locating pin C to lock the support in various angular settings to suit the operations to be performed.

> A partly-machined casting is loaded to the work-support through one side of the stirrup-shaped frame, and the bored end is engaged with a spigot on the end plate. The angular disposition of the casting is controlled by two pegs that project from the end plate, and engage a flat at one side of the

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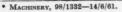




Fig. 1. An air separator body on which drilling, tapping and spotfacing operations have been performed is seen in the foreground. In the background at the right, is shown a component after the preceding operation stage performed on a Ward turret lathe, and at the left, an unmachined casting

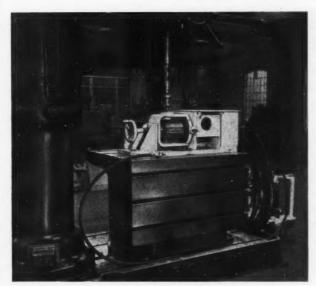


Fig. 2. The set-up on an Archdale radial machine for drilling, spotfacing, and tapping air separator bodies at the Crayford works of Vickers Armstrongs (Engineers), Ltd.

cast flange. Thus positioned, the casting is secured by a clamp pad D, which is pivotally mounted on a screw that passes through the left-hand end bearing for the work-support, and is advanced or retracted by turning the handwheel E. When the workpiece has been clamped, additional support is provided by bringing a screw-operated jack-pad F into contact with the casting, in line with—but on the opposite side to—the large facing.

The main frame of the fixture houses five Aro-Broomwade Par-A-Matic type PO-14-2A air operated drilling units (as described in MACHINERY, 94/605—18/3/59), and the ends of these units are indicated at G. Each

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unit is held in a split circular clamp, and secured by a single socket-head screw, so that it can be readily removed if required. In Fig. 3, the hinged cover that normally encloses the top of the main frame is raised, and the ends of the drilling units can be seen through the circular opening in the frame side member, also below. By setting a control knob, each Par-A-Matic unit can be arranged to operate in accordance with any one of three systems, as follows: —(a) from a single air line which supplies both the spindle drive motor and the built-in feed cylinder, a constant drilling feed

rate then being obtained, with spring return of the spindle; (b) from two air lines, one of which serves the drive motor and the other the feed cylinder, the feed and return rates then being the same, and steplessly adjustable, by means of a needle valve, from 0 to 8 in. per sec.; and (c) from two air lines, with adjustable feed rate and spring return of the spindle. The third arrangement is employed by Vickers Armstrongs, and the spindle of each unit is run at 1,400 r.p.m. and is

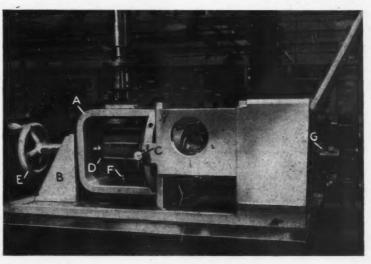


Fig. 3. Close-up view of the fixture on the Archdale radial drilling machine. At the right may be seen the air-operated tools for drilling the holes in the flange while the other operations are being performed



Fig. 4. This multiple tool is employed on the Archdale machine for boring, spotfacing, and chamfering a hole in each air separator body

fitted with a chuck of fe-in. capacity. Operations on the Archdale machine are performed in two stages. First, with the fixture in the position shown, the large hole is bored, spotfaced, chamfered, and tapped, and one of the smaller holes is drilled and tapped. During these operations, the automatic cycle of the Par-A-Matic units is started, and five of the holes in the flange are drilled. Next, the work-support of the fixture is inverted, and the remaining small hole is drilled and tapped. At the same time, five more holes are drilled in the flange by the Par-A-Matic units. Drills used in these units have points of 140-deg. included angle, to ensure that they break through the flange cleanly. The end of the fixture which houses the Par-A-Matic units is padded with polythene foam material, in order to reduce noise.

The combination cutter used for the boring, spotfacing, and chamfering operations is seen in Fig. 4. It has a steel body fitted with four bronze pads H that bear against the bore of the

large guide bush in the work-fixture. There are four boring teeth, as at J, formed by wedge-type inserts, and four spotfacing teeth, of similar type, as at K. A single tool-bit L provides for chamfering. The inserts and tool-bit were supplied by English Steel Tool Corporation, Ltd., and are provided with brazed on tips of Escalloy tungsten carbide.

AIR SUPPLY TROLLEY

For controlling the air supply to the Par-A-Matic units there is a lever-operated valve at the rear of the fixture base, adjacent to the clamping handwheel. This position was selected to ensure that the lever is not inadvertently reset by the operator while loading or changing the tools in the spindle of the Archdale machine. Compressed air is delivered to the units by way of flexible hoses connected to outlets on a special trolley, which is just visible at the right in Fig. 2.

A close-up view of the trolley, which was designed and built by Vickers Armstrongs, is given in Fig. 5. It has a wooden base with two rubbertyred wheels, and steel frames at either end support the manifold pipes and other units. Air is delivered to the trolley by way of pressure hose M, of 1-in. bore, which is connected to the shop

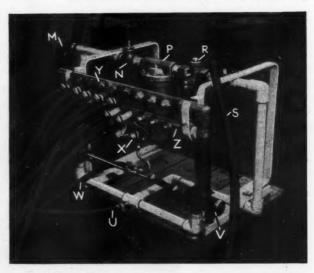


Fig. 5. This air supply trolley has been developed by Vickers Armstrongs (Engineers), Ltd., for the control and delivery of compressed air to the tools in the fixture on the radial drilling machine. [Incorporating valves, filter, lubricator, and multiple outlets, it can be used for other duties

air supply line by a quick-release coupling. The hose is connected to the upper, central, run of pipe on the trolley, and this pipe incorporates a main shut-off valve N, a Norgren filter P and a Norgren lubricator R. On the "downstream" side of these units there is an outlet for the delivery of air to the hose S which serves a blow-gun on the machine.

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The air supply pipe connects with a T-piece at the front of the trolley base from which an outlet *U* provides for the delivery of air to the control valve on the fixture. From the T-piece, pipes branch outwards to the inlet connections of two valves, as at *V*. These Maxam 3-way, pilot operated, automatic return valves are

matic return valves are of the "normally off" type. A hose W from the Maxam control valve on the fixture is coupled to an adapter, from which connections lead to the pilot inlets of the 3-way valves, also to the pressure reducing valve X. When the control valve lever is moved to engage the Par-A-Matic units, air

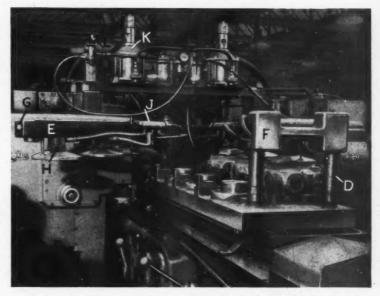


Fig. 7. The set-up on a Cincinnati duplex machine for milling the feet on six main pump bodies at one setting. The fixture has air-hydraulic clamping arrangements

passes to the 3-way valves, which are reset to connect the main inlets to the upper manifold pipe Y. At the same time, air passes through the reducing valve to the lower manifold pipe Z. Each manifold pipe has eight outlet connections, only five of which are used for this application,

and hoses lead from the manifold Y to the inlets for the motors of the Par-A-Matic units. Hoses from the manifold Z connect with the feed cylinder inlets of the units, and the thrust applied to the drills can be regulated by adjusting the reducing valve X on the trolley.

MILLING MAIN PUMP UNIT BODIES

Bodies for the main pump units of the petrol dispensing pumps are machined from grey iron castings. Two castings

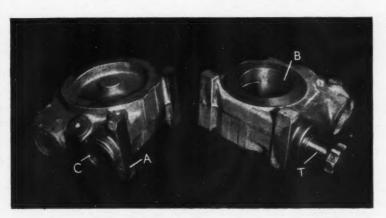


Fig. 6. A main pump body is seen at the right, with a locating plug in position, before the milling operation on the feet. At the left is seen a milled casting



Fig. 8. Close-up view of the fixture on the Cincinnati milling machine, showing the locating and clamping units for the main pump bodies

at different stages in the machining sequence are seen in Fig. 6, and it will be noted that there are two rectangular feet which are face milled as seen at A on the casting at the left. Face milling is performed on six castings at a time on a Cincinnati Hydromatic duplex machine, and the machining operations which precede the milling stage have been completed on the casting at the right. These operations include machining of the main bore B for the pump rotor, and the adjacent face; boring a transverse hole-seen at C in the casting at the left-for a relief valve; pressing-in a bronze bush, at the same set-up on a turret lathe; counterboring the outer end of the hole; machining the surrounding face; and cutting a thread for a sealing cap.

Fig. 7 is a general view of the Cincinnati machine, which has a 42-in. long table, with a traverse of 36 in. under automatic control. The machine is arranged for climb milling and the two spindles are fitted with Escalloy cutters of 6 in. diameter, which have wedge-clamped, carbide-tipped, inserted teeth. Each cutter has 12 teeth, and the geometry of the cutting edges gives 15 deg. negative radial rake, 15 deg. positive axial rake, zero true rake, 45 deg. corner angle and 12 deg. positive angle of inclination. The cutters are run at 167 r.p.m., and the table is fed at a

rate of 8 in. per min. for cutting, the thickness of metal removed ranging up to % in.

A massively proportioned fixture is secured to the machine table, and accommodates six components in two rows. The fixture is arranged for hydraulic clamping, by PowRlock Junior units supplied by Spencer, Franklin, Ltd. (MACHINERY, 92/1178 -16/5/58). At each end of the fixture base there are pairs of stout pillars, as at D, and on the pillars at the far end of the base (as viewed in Fig. 7) are pivoted two beams, one of which is indicated at E. A bridge member F is fitted to the nearer pair of pillars, and has a slot at each side with which a beam can be engaged. In the end of each beam is fitted a large diameter ball, as at G, which is urged outwards by a spring, but retained by a plate. When the beam is engaged with the slot in the bridge member, the ball enters a groove to retain it in position.

Each beam carries three clamping units, incorporating PowRlock heads as at *H*. The heads are connected

by flexible hose to a manifold J, secured to the beam, and each takes the form of a hydraulic cylinder with a hollow ram, which has a bore of in. diameter. Pressure oil for the heads is supplied to each manifold from an air-hydraulic booster, as at K, by way of flexible tubing, and each booster is connected to the shop air supply by large-bore hose. The boosters are mounted on a cross-member that spans the columns of the machine, and this member also carries Norgren filter and lubricator units and a pressure reducing valve, also a Maxam lever-operated valve L for controlling the air supply to the boosters. With the pressure of the air supply to the boosters set at 40 lb. per sq. in., a force of 800 lb. is applied by each head, the maximum clamping stroke being

Details of the clamping and location arrangements for the workpieces are seen in the close-up view in Fig. 8. Each casting is clamped by a plate with three pads, and most of the plates are circular, as seen at M. The plate for the casting at the far end of each row (as viewed in Fig. 7 and 8) is cut away, and one of these plates is seen at N. A large V-shaped notch embraces the headstock casting at that side of the machine when the beam is swung outwards, and thus permits additional movement. The large flat at the other

side of the plate ensures that there is ample clearance for loading and unloading the workpieces. Each plate is fitted with a vertical pin which enters a hole in the beam and prevents rotation. The plates are mounted on universal swivelling joints at the ends of studs that pass through the PowRlock heads. Each stud extends through a hole in the beam into a counterbore, and is urged upwards by a compression spring which acts against the bottom of the counterbore and the lower face of a nut fitted to the upper The arrangement is such that when pressure oil is applied to the PowRlock head, the plate is thrust downwards, compressing the spring, and the latter lifts the plate when the oil supply is cut off. Each counterbore is closed by a small circular cover plate to prevent the ingress of swarf and dirt.

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nits her On the fixture base there are work-support blocks, each with a spigot, as at P, and a horizontal seating face. A casting is loaded so that the previously-machined rotor bore (B, Fig. 6) engages the spigot, and the face surrounding the bore rests on the seating. At one side of each support block, there is a vertical pillar with a knurled-head screw, the pillar for the block P being seen at R. In line with the screw, and secured to a facing on the fixture base, there is an L-shaped location block S. When a casting is loaded on to the support block, a special plug, fitted in the previously-machined relief-valve bore, extends over the block S, and

pressure is applied to the casting by the knurled-head screw to swing the workpiece about the spigot *P* until the plug contacts the vertical limb of the block. The pump body is then located with the relief valve bore in line with the travel of the table, and the clamps are applied.

A locating plug is seen fitted to the casting at the right in Fig. 6, and it has a threaded portion which is a slack fit in the thread machined in the casting. Location is taken from the plain portion of the plug, indicated at T, and at the end of this portion there is an integral flange. flange contacts the machined face at the outer end of the relief valve bore when the plug is fully screwed home, and ensures that the portion T is at 90 deg. to the face. Locating plugs are fitted to a batch of six castings, at a bench adjacent to the Cincinnati machine, while another batch is being

It may be of interest to mention

that when the full clamping load is applied to the six castings, the maximum deflection of the beams is 0.030 in. The floor-to-floor time now required for milling six main pump bodies is 21 min., as compared with 27 min. when the work was hand-clamped.

MILLING SLOTS IN ROTORS

Rotor bodies for the main pumps are made from cast iron, and each has six equally-spaced radial slots, which are 0·188/0·190 in. wide by 1½ in. deep. The slots are milled on an Archdale 18-in. production type machine, after the body has been turned, faced, and bored, and side-and-face cutters are used, each of which has 14 teeth tipped with Escalloy tungsten carbide. A close-up view of the set-up is given in Fig. 9, and the rotor bodies are milled four at a time, two being mounted on each spindle of a 2-spindle indexing fixture.

This fixture is of simple construction, the work-carrying spindles being carried in a block U at one end, which is integral with the base. Both spindles have gear teeth which mesh with an intermediate gear, so that they can be rotated together by means of a tommy-bar inserted in holes in the flange of either unit. Separate locating plungers are provided for each spindle, as seen at V, and engage bushed holes in the flanges. At the end of the fixture base remote from the block U there are lugs, between which is pivoted a bar W. This bar carries two retractable centre points, which are

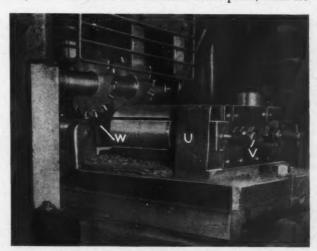


Fig. 9. At this set-up on an Archdale machine, six slots are milled in each of four main pump rotors at one setting. A 2-station indexing fixture and two carbide-tipped cutters are employed



Fig. 10. An unmachined light-alloy casting for a component known as a clock case is seen at the left, and a casting which has been milled on the end faces, at the right

engaged with centre holes in the ends of the spindles, to support them during the milling operations. For loading, the centre points are withdrawn and the bar is swung upwards to afford access to the spindles. Two blanks are then loaded

on each spindle and clamped by means of a nut and washer.

For the milling operations, the cutters are run at 150 r.p.m., and the table is advanced at a feed rate of 2½ in. per min. The time required for milling the six slots in four workpieces is 9 min., and 1,400 components can usually be milled before the cutters need to be resharpened.

MACHINING LIGHT ALLOY CASTINGS

Part of the mechanism for the petrol pumps is housed in an aluminium alloy casting, known as a clock case. An unmachined casting is seen at the left in Fig. 10, and it will be observed that it is of thin section, with numerous cored openings, so that special attention must be paid to supporting and clamping during machining operations. Particular care is necessary in connection with the milling of the end flanges X, and a casting is seen at the right after these flange faces have been machined.

The flange faces are milled simultaneously on an Archdale duplex machine, and a view of the set-up is given in Fig. 11. It should be mentioned that certain guards have been removed in order that details of the fixture and cutters may be more readily observed.

Before the milling operation on the Archdale machine, a facing inside the box portion of the casting is milled for location purposes, as indicated at Y in Fig. 10, and the bottom face of the box portion (seen uppermost on the part at the right) is also machined to ensure a good seating surface.

A fixture of welded construction is provided on the Archdale machine, and it has a beam, of inverted-U shape, pivoted in a block at one end. This beam is indicated at A in Fig. 11, and the end remote from the hinge is located by a slot in

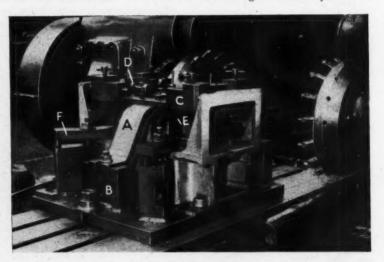


Fig. 11. A view showing the fixture and cutters designed and made by Vickers Armstrongs (Engineers), Ltd., for milling the end faces of "clock cases" on an Archdale duplex machine

a block B, on the fixture base, and secured by a nut and eye-bolt. On the beam is mounted a frame with blocks—as at C—at each corner. Each block houses a sliding plunger, which is urged outwards by a spring, and each plunger can be withdrawn into the associated block, and held in the withdrawn setting by turning it through 90 deg. The inner end of each plunger is fitted with a finger lever, and each block is provided with a thumb-screw whereby the plunger can be locked in place. At each side of the frame, between the blocks, there is a screw and lock nut, as at D. These screws serve to steady the casting during the milling operations.

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The beam A, and with it the frame assembly, are swung clear for loading, and a casting is mounted in the fixture with the bottom face of the box portion resting on the base, as shown. The beam A is then swung into the working position, and is lightly secured by the eye bolt and nut of the block B. Below the beam there is a wedge shaped block E, which is engaged with the clevis member Z, Fig. 10, to locate the casting transversely. The casting is then thrust endwise by a hand-operated screw in the pivot block for the beam, so that the machined face Y contacts a location member on the base of the fixture.

With the casting thus positioned, the beam is finally secured, and clamps, as at F in Fig. 11, are applied. These clamps, it may be noted, make contact with the casting immediately above the corners of the box portion to reduce the risk of distortion. The screws at each side of the frame are advanced into contact with the workpiece until they are "finger tight", and are locked in position. Finally, the levers of the spring plungers are moved to the vertical positions shown, so that the plungers are released, and urged into contact with the casting by the associated springs. These plungers serve as vibration dampers during cutting, and they are secured in their working settings by the thumb screws.

For the duplex facing milling operations, Vickers Armstrongs have made the special cutters seen in Fig. 11. Each has a steel body with angularly-disposed holes to receive 16 Escalloy carbide tipped boring tools, supplied by English Steel Tool Corporation, Ltd. Screws in the cutter body provide for adjusting the tool bits endwise and for clamping them in the seating holes, and the bits are set so that the points of the carbide tips are on a 10-in. diameter. The cutters are run at a speed of 365 r.p.m. for the face milling operation, and the work-table of the machine is traversed at a feed rate of 5 in. per min.

Another article on the production of petrol pumps will be published shortly in Machinery.

Simplified Bonus Clock

Bonus Clocks, Ltd., 5-7 Church Road, Richmond, Surrey, have now introduced a version of the Robinson "bonus clock" which is cheaper and



"Earnie" bonus clock, introduced by Bonus Clocks, Ltd.

simpler than that described in Machinery, 98/217—25/1/61. Known as "Earnie," this recording clock, which is of patented design, does not show the actual bonus time or cash earnings, but informs the operator immediately if a longer time is being taken over an operation than that for which the dial is set. A green lamp is illuminated during the period for which the clock is set, and a red lamp when this time has elapsed.

The standard bonus clock already described has a range of 15 sec.-10 min., but this modified type can be supplied with ranges of 3 to 15 sec., 15 sec. to 4 min., and 30 sec. to 12 min. A built-in electro-magnetic counter with hand re-set can be provided, and a floor stand is available. The cast aluminium housing of the clock measures 8 by 6 by 9 in., or 11 by 6 by 9 in., if a counter is built-in.

If it is considered undesirable for an operator to be able to alter the dial setting, the instrument can be supplied with a removable key in place of the knob. It has been found, however, that very good results have been obtained by allowing the operator to adjust the setting knob until the best working pace has been ascertained. Increases in output of between 20 and 40 per cent are stated to have resulted from this procedure.

Standardization of Machine Tools in East Germany

By R. E. GREEN, Associate Editor

REFERENCE TO THE ORGANIZATION and the scale of operation of the machine tool industry in East Germany was made in Machinery, 99/202—26/7/61, in an article primarily concerned with the Institute of Machine Tool Engineering in Karl-Marx-Stadt, and the work undertaken there. In this article, other activities of the Institute are considered, including the development of a system of unit construction for machine tools, and efforts to increase the productivity of the machine tool-using industries.

THE PRINCIPLE OF UNIT CONSTRUCTION

Attention was drawn in the previous article to the adoption of the so-called unit construction system by machine tool factories in East Germany. In this connection, much of the impetus has come the application of the system on a national basis will be awaited with interest.

One of the first machines to which unit construction principles were applied was the centre lathe, which is made in various types and sizes by a number of East German factories. Working in conjunction with the Institute, the designers of these companies have modified their machines so as to incorporate components and assemblies with standardized dimensions. The simplest application of the system is to a centre lathe made in only one size, which may be designed to incorporate, for instance,

from the Institute, where the system is seen as

affording a further contribution towards the reduc-

tion of costs and the raising of efficiency within the industry. While the idea is by no means new, the use of standardized components for the con-

struction of a range of equipment has been largely

confined hitherto, in the Western countries, to the

products of individual factories, and the results of

made in only one size, which may be designed to incorporate, for instance, any of four headstocks, all of which have similar dimensions. These headstocks are so designed that the same casting can be employed for all, and the number of castings required makes it possible for larger batches to be handled on special equipment such as multi-way drilling and boring machines.

On assembly, the headstocks may be fitted with gear arrangements to provide restricted, normal, or wide speed ranges, and with equipment for the selection of speeds by levers, magnetic clutches, or hydraulic cylinders under remote control, or with steplessly-variable speed drives. Similar arrangements may be made as regards feed gearboxes, which may incorporate only feed gears, or feed gears with provision for thread-cutting, and gear-changing by levers or under remote control. A range of interchangeable spindles, for use with various types of chucks, to be operated by pneumatic, hydraulic or

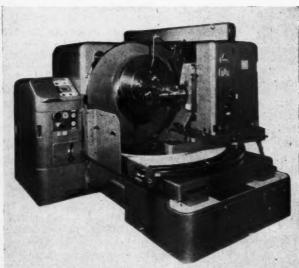


Fig. 1. This spiral bevel and hypoid gear generating machine, built by the Modul factory in Karl-Marx-Stadt, is designed for roughing operations, and is one of six machines in which the same basic elements are employed

electric power, or by hand, may be provided, and the tailstock may also be arranged for hand or

power operation.

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The saddle is designed for use with a range of equipment including the normal cross-slide with compound rest, tool turrets with either vertical or horizontal axes, cutting-off tool-holders, and copying slides. With such a range of standardized units it is possible to build a wide variety of lathes, and standard or special machines can be provided at relatively low cost. Examples of lathes built from components or assemblies such as those mentioned were shown at the Leipzig Fair by the 8th May factory, and were described in MACHINERY, 98/939—26/4/61.

From the use of standardized parts for one size of machine, the next step is to re-design certain parts so that they can be incorporated in two or more different sizes. For instance, by slight increases in the dimensions, a lathe spindle suitable for a 6-in. swing lathe is used in an 8-in. version of the machine. The spindle is then somewhat heavier than is necessary for the smaller machine, but economies in production costs, and the possibilities of using auxiliary equipment such as chucks and the associated operating mechanisms on both sizes of lathe are expected to offset this drawback.

Another aspect of the unit system is the possibility of employing standardized sets of gears, made in a wide range of diameters and pitches, with splined bores of standard sizes. Such gears could be produced by the most efficient modern methods on production lines of the type employed in motor vehicle plants, and designers would be encouraged to incorporate them in all new designs of machine until they became fully integrated into machine tool building.

UNIT CONSTRUCTION OF GEAR-CUTTING MACHINES

Because the various types of bevel gears employed in such large numbers in the motor vehicle industry fall within a fairly narrow size range, only one size-or at most two sizes-of bevel gear cutting machine is built, although a variety of types is required to suit the cutting processes to be employed. The largest factory engaged in building gear cutting machines in East Germany is that of Modul, in Karl-Marx-Stadt, and the range of bevel gear cutting machines made by this company now includes six types, all of which incorporate standardized units. An example is the ZFTKKR 500 by 10, spiral bevel and hypoid gear generating machine, intended for roughing operations on gears up to 14 in. diameter, which is shown in Fig. 1.



Fig. 2. The basic elements of the range of bevel gear-cutting machines made by Modul include the bed, drum housing, table, and a support beam (not shown)

An assembly of some of the standardized units employed in this range of gear-cutting machines is seen in Fig. 2, and it incorporates a base casting with machined surfaces on which housings for the various mechanisms are carried. The large housing at the rear has a circular aperture in which can be fitted spindle-carrying drums of five different types, depending on the design of machine required. To the left of this housing there are surfaces to carry the roll drive gearbox, which may also take several forms. The swivelling table, which is also standardized on all six machines, is carried on guide-ways in front of the large housing.

Several designs of work-spindle housing may be fitted to the table to suit the type of machine to be constructed and the completed assembly may incorporate equipment for hydraulic clamping of the work, stepless feed regulation, automatic changing of the feed rate for roughing and finishing passes, and an automatic chip conveyor in the base. The support beam fitted at the top of the machine in Fig. 1, between the cutter- and the work-spindle housings, is also standardised, and may be fitted to any machine on which it is required. Although the range of six machines must obviously include many special components and assemblies, it is evident that considerable economies may be expected to result from the ability to machine the

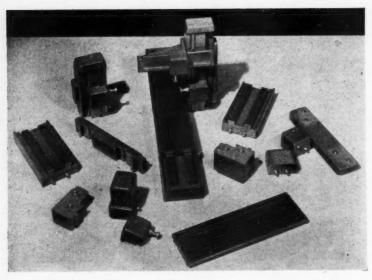


Fig. 3. These models show the basic elements and several of the common components and assemblies from which plano-milling machines of various types can be built up

heavier castings in batches of larger quantities. The Modul factory has also applied the unit construction principle to the design of gear-shaping machines of two sizes, with capacities for gears of 9.8 and 19.68 in. diameter. It is calculated that the total cost savings likely to result from reductions in the time required for design, in foundry patterns, and in the time required for setting up for machining (because of the larger batches handled) will be of the order of 40 per cent. At present, however, the pressure of work in the Modul factory, and in other machine tool plants where unit construction methods are employed, is so great that there has been little opportunity for building the special machines and fixtures required to enable full advantage to be taken of the system.

Plano-milling and planing machines also lend themselves well to construction from basic units, which include the bed, right- and left-hand columns, cross-beam and cross-rail, and cantilever cross-rail. These basic units, examples of which are shown in model form in Fig. 3, are used in conjunction with other components and assemblies such as tables, table-drives, right- and left-hand milling spindle heads or cross-slides, and slide adjustment drives. When automatic operation of such a machine is required, extra—specially-designed—equipment is added to the standard assembly.

As mentioned in MACHINERY, 98/1077-10/5/61, the Naumburg factory has recently introduced a range of units standard which a variety of vertical honing machines can be assembled for specific purposes. The range of basic units includes columns, recbases, tangular and circular tables in several alternative sizes, and singleand twin-spindle heads, and the machines can be fitted with equipment that provides for either semi-automatic or fullyautomatic control.

UNIT SPINDLE HEADS

To enable automatic transfer machines of the in-line and rotary types, also multi-way drilling

and tapping machines to be built economically, a range of unit spindle heads and associated bed, column and table units, feed slides and other equipment, has been introduced, which provides for such operations as multi-spindle drilling and tapping, boring, fine-boring, milling and face-grinding. These heads have been designed in collaboration with the Institute by the John Schehr factory in Leipzig, where milling and plano-milling machines and milling heads are made; by the Saalfeld drilling machine factory; by the Vogtland factory at Plauen which supplies a complete range of heads in a variety of sizes; and by the Mikromat factory in Dresden where grinding heads are produced.

The travelling-type milling head seen in the background in Fig. 4 is from the Vogtland range, and was exhibited at the Leipzig Fair, together with the model of an in-line transfer machine in the foreground. Of conventional design, the milling head can be supplied with a single spindle speed, to suit the application, and a single feed rate. Control equipment is also available whereby the head can be arranged to operate on a rapid advance, machining feed, and rapid return cycle, which can be synchronized in the automatic cycle of the complete machine.

Unit boring heads, from the Vogtland range, are incorporated in the 3-way boring and facing machine in Fig. 5, which was designed for opera-

tions on three slightly different iron castings for lorry gearboxes. These heads have facing slides which are operated through helical rack and pinion systems powered by hydraulic cylinders, as seen at the right-hand end. The small electric motor above the cylinder provides for small increments of movement at slow speeds when setting-up.

EQUIPMENT FOR LINKED MACHINE LINES

As mentioned briefly in Machinery, 98/1075—10/5/61, equipment has been developed by the Institute, in collaboration with several factories, whereby a

number of different machines, each working on an automatic cycle, can be arranged for automatic loading and unloading. Examples of such equipment have already been described, notably

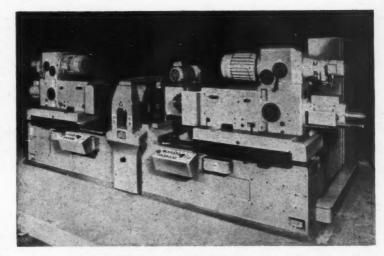


Fig. 5. Standard fine-boring heads, with equipment which includes radially-fed facing slides operated by hydraulic cylinders, are incorporated in this 3-way machine for operations on gearbox castings

in connection with a link-line for the production of electric motor shafts (MACHINERY, 95/213—12/8/59). Since that article was published, the line has been installed in a factory at Nieder-

sedlitz, where it has been supplemented by equipment designed to roll serrations on the shaft periphery to retain the armature, and to press the armature into position.

Equipment needed for such a line includes convevors to carry the work the unloading position of one machine to the loading position of the next, and an automatic unit which has been designed by the Institute for this purpose is shown in Fig. 6. This particular unit is arranged for handling shafts, which are transferred from a position at the left by a double roller - chain conveyor, provided with V-blocks. The conveyor is indexed



Fig. 4. Typical of the range of milling units available is this AF 3 travelling type head, suitable for use in in-line transfer machines such as that seen in model form in the foreground

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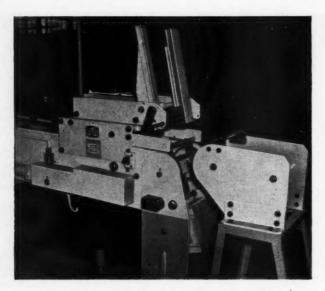


Fig. 6. Developed by the Machine Tool Institute, this unit forms part of a complete standardized system designed for linking automatic-cycle machine tools to provide fully-automatic production lines

automatically, by successive movements of an air cylinder ram, and shafts are thus brought, in turn, into a position above two other V-blocks on the ends of a horizontal bar.

The bar is attached to the ram of an inclined air cylinder, and when this cylinder is operated, the shaft is raised into the guide-ways of a nearly-

vertical magazine above. Springloaded retainers hold the shaft when the cylinder ram is retracted, and the magazine is arranged to hold a number of shafts to provide a buffer stock. When the next machine in the line completes a cycle and calls for another shaft, a third air cylinder is operated, to push the magazine to the right, horizontally, towards the loading station of that machine. In Fig. 6, this station is represented by the small unit at the right, which carries two more V-blocks, each having a sloping surface on one side.

As the magazine is advanced, the lowest shaft in the chutes rides up these sloping surfaces and then descends into the V-grooves, in which it is retained when the magazine is

retracted. The transfer equipment of the next machine is then brought into operation to carry the shaft to the chucking or clamping position.

SPECIAL TOOLS

Engineers of the Institute have also carried out investigations in connection with tools of the type employed for machining multi-diameter bores, and some standard designs in which the cutters can be adjusted to various positions in both the axial and radial directions have been developed. Much of this work has been concerned with tools which enable roughing, semi-finishing, and finishing operations to be carried out at a single pass, and an example is shown in Fig. 7.

The drill illustrated has separate lands of two different diameters, which serve to drill the hole from the solid and take a semi-finishing cut. Further advance of the drill then brings into operation a solid carbide blade A, which is clamped in a slot in the tool shank. The blade can be arranged to cut on one or both edges,

and if only one edge is used, provision can be made for taking up wear, also for compensating for metal removed in regrinding, by means of a back-up or rubbing pad on the side opposite to the blade. Experiments have shown that holes with a finish of 40 micro-inches can be produced consistently, over long periods, with such a tool.

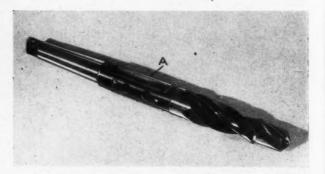


Fig. 7. Work undertaken by the Institute includes the development of tooling of various types. This combination drill is fitted with a blade A, of solid tungsten carbide, which provides for reaming, after the hole has been drilled in two stages

Pinch Trimming and Swaging Dies for Covers

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By M. J. GOLDSTEIN

Shown below in Fig. 1 are the stages involved in the production of the jar cover A from 0.020 in. thick mild steel sheet. The blank size for this component is 3% in. diameter, and the press tool for the first operation produces the drawn, trimmed, and pierced shell at B. A feature of this tool is that it is arranged to pinch trim the component, to avoid the need for a separate trimming operation. The scrap produced by pinch trimming is indicated at C.

As may be seen in the drawing, Fig. 2, the construction, in general, follows normal practice for blanking and drawing tools, but the punch over which the blank is drawn consists of two members, D and E. The part E is curved to produce the required form on the component, and it incorporates a die insert for the pierced, $\frac{1}{6}$ -in. diameter, hole in the top of the workpiece. The recess in

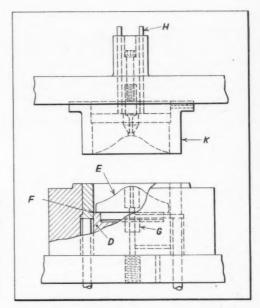


Fig. 2. Part-sectional view of the blanking, forming and pinch-trimming tool for the mild steel jar cover A, Fig. 1

the top of the part D is made $\frac{1}{16}$ in. deeper than the length of the shoulder on the member E, to allow for regrinding the trimming edge at F. A bush G is provided

in the member D, which makes contact with the lower face of the part E, to prevent the in. diameter scrap piercings from the centre hole becoming jammed in the 16-in. clearance space, When the pinch trimming surface is reground, the same amount is removed from the top face of the bush G. The punch for the centre hole has a 1/2-in. diameter shank and is held in the top tool by means of a socket-head screw. Two knock-out pins are provided at H, and both the blanking punch K and the die member D have

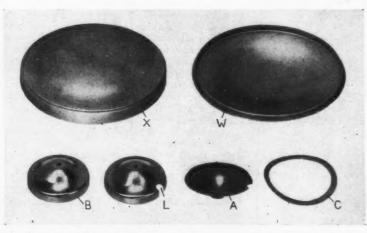


Fig. 1. Production stages for a casserole cover W, and a jar cover A. Blanking, drawing and pinch-trimming and rim swaging tools are employed

drilled air vents. Air vents are also provided in the member E to assist stripping.

A slot is required in the cover, as shown at L in Fig. 1, to accommodate a spoon, and is produced with the tool shown in Fig. 3. Here, the workpiece is located on the profiled steel block M, by means of a pin which engages the 36-in. diameter centre hole. In making this tool, a turned, 11/2-in. diameter shank was first provided on the block M, and a slot was milled to accommodate a cast-steel With the latter fixed in position, the block was finish machined on the profile, and the centre hole drilled and reamed for the location pin. Finally, the block was milled to an angle of 45 deg., for mounting on the bolster plate. After the required profile had been machined in the die insert N, and a clearance hole provided in the block M, the rough-machined punch P was finished by shearing it in the die opening, and removing excess metal by filing. It will be noted that the punch is provided with a heel which enters the die aperture before cutting starts, to prevent deflection.

The swaging operation, to bring the component to the stage seen at A, in Fig. 1, is performed in the tool shown in Fig. 4. Since no cutting is involved, pillars are not provided for this die set. The die ring R, of oil-hardened tool steel, has a recess of the same bore as the outside diameter of the component. The depth of this recess is % in.,

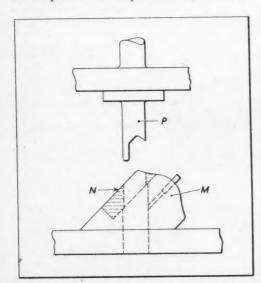


Fig. 3. Press tool for cutting the spoon slot in the jar cover

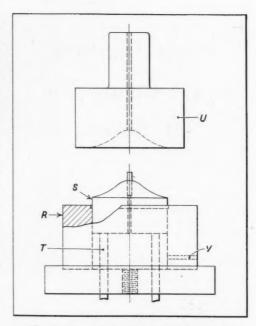


Fig. 4. Press tool for producing the swaged rim on the jar cover

which is the same as the length of the shoulder required on the component after it has been swaged. The formed centre member S, which is provided with a location pin for the work, is a sliding fit in the die ring R, and is supported by four pressure pins T. The latter bear on the steel top washer of a rubber pressure pad carried on a %-in. diameter rod screwed into a tapped hole in the bolster. The height of the pressure pins is such that when the workpiece is placed in position on the centre member S, the lower edge of the piece rests on the bottom of the recess. when the punch U moves down and makes contact with the work, the excess metal can only move outwards and form the required swage shoulder. A vent hole V is provided in the ring member to prevent air lock.

A somewhat similar component, but of larger size, is shown at W in Fig. 1. This casserole cover is made of 0.020-in. thick brass sheet, the blank size being 8% in. diameter. The part is brought to the form shown at X in a tool of similar design to that employed for the cover B, the amount trimmed off by the pinch action being about % in. The swaging tool is also of similar design to that shown in Fig. 4.

Machine Shop Patents

OPTICAL INSTRUMENT FOR MEASURING ANGULAR SETTINGS

Intended for accurate measurement of angular settings of the swivelling head on a vertical milling machine, the instrument shown sectioned in the accompanying side elevation has a taper spigot, whereby it may be mounted on the nose of the

spindle.

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The entire instrument is thus inclined when the head is swivelled, and the disc A, which is co-axial with a pin that is pivotally-mounted in the fixed bush B, is then turned back to a datum position. This position is obtained by reference to a bubble level, which is secured to the outer face of the disc, and the motion is imparted by means of a worm, which engages teeth on the periphery of the driving ring C, attached to the rear of the disc. Measurement of the angle through which the disc has been turned is obtained with the aid of a micro-

Sectional view of an optical instrument for measuring angular settings of a swivel-type vertical milling head

scope, mounted on the disc, whereby markings on the glass scale ring D are observed through a graticule which is graduated in divisions of 1 min. or arc. The scale ring D is supported by a flanged plate, which is pivotally-mounted on the periphery or the bush B, and is normally held stationary in relation to the case. To provide for adjustment of the zero position, however, the assembly may be turned by means of worm screws.

To facilitate reading, the scale ring is illuminated by light which passes through an arcuate slot in tne rear of the case, and then through a window in the ring E, which is screwed into the driving ring When the instrument is being set up, the ring E is turned independently to a second position, motion being transmitted from the operating knob F by a shaft that extends through an arcuate slot in the scale ring carrier and has a pinion which meshes with teeth in the bore of the ring. In this way, a prism mounted on the ring is brought into line with the optical axis of the microscope, as shown in the drawing, to permit observation directly below the instrument, through a magnifying lens, housed in the driving ring. By turning the instrument about the vertical axis, it is adjusted to a position such that diametricallyopposed pairs of lines on the microscope graticule straddle the image of any transverse edge on the machine, to ensure that the plane of the scale ring is parallel to that in which the spindle head swivels. Clamping screws, whereby the instrument is secured to the taper spigot, provide for horizontal adjustment, for aligning the axes of the vertical optical system and the spindle.

864,575. Karl Miller, 6 Kochstrasse, Innsbruck, Austria. [Application date in Austria May 6,

1958. Published April 6, 1961.]

FEED MECHANISM FOR A TAPPING MACHINE

The arrangement here described is intended primarily for incorporation in the feed mechanism of a tapping machine of the type whereby the feed and return movements of the spindle are obtained as a result of the engagement of a threaded portion with a nut, the spindle being rotated at faster and slower speeds, respectively, than that at which the nut is constantly driven. It serves to ensure that axial movement to bring the threaded portions together at the beginning of an

operating cycle is not imparted until the first threads on the spindle and nut are in such angular

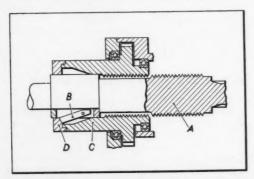
positions that they will engage smoothly.

In the accompanying sectional view, which shows part of the mechanism within the spindle head, the spindle A is shown in the position which is occupied after the completion of an operating cycle. A pawl B, which is pivoted in a longitudinal slot in the spindle, is enclosed within an annular extension at the left-hand end on the feed nut C. During the idle period after the completion of a cycle, the spindle is rotated at the speed employed for the feed stroke, and the pawl is thus held outwards by centrifugal force. When a tresh cycle is started by means of a cam-operated lever, the spindle is traversed to the left until the pawl contacts the inner face of a ring D, which is attached to the outer end of the feed nut exten-Additional movement of the lever then serves to compress a spring which urges the spindle in the same direction.

The inner face of the ring is bevelled, and over an arc of 180 deg. the angle of inclination is such that the line of the force resulting from the spring pressure passes through the pawl pivot, the assembly thus being held stable to prevent axial movement of the spindle. Rotation of the spindle with respect to the nut subsequently brings the pawl into contact with a different portion of the bevel, which is at such an angle that the line of force passes between the pivot and the spindle axis. The pawl is then thrust into the slot, and the spindle is allowed to move to the left, under the spring pressure, in a pre-determined angular

relationship with the nut.

The operating lever is returned while the tapping cycle is in progress. A second spring serves to move the spindle clear of the nut, during the



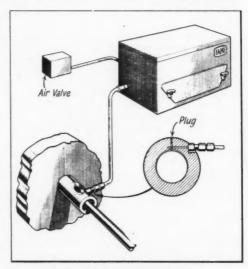
Feed mechanism for a tapping machine designed to ensure smooth engagement of a thread on the spindle and a rotating nut

final stage of the retraction stroke, after the threads have disengaged.

854,533. Wickman, Ltd., Banner Lane, Tile Hill, Coventry. (Inventors, Mr. R. J. Dixon and Mr. L. Jones.) [Application date, March 25, 1958. Published, November 23, 1960.]

Fame Automatic Lubricant Injector

The Foundry & Metallurgical Equipment Co., Ltd., Netherby, Queen's Road, Weybridge, Surrey,



The Fame automatic lubricant injector

are producing the Fame automatic lubricant injector for applying graphite compounds and other suitable lubricants to the surfaces of mating plungers and sleeves in pressure die casting This equipment, which is shown in simplified form in the accompanying figure, comprises a supply tank and a 2-stage air-operated pump designed to deliver metered quantities of lubricant at a final pressure of 1,500 lb. per sq. in. to a connector screwed into the sleeve of the die casting machine. Pump displacement is controlled by steel distance pieces which may be set to control the delivery of lubricant at each stroke from a minimum of 0.005 cu. in. to a maximum of 0.045 cu. in. The equipment is operated by compressed air at 60-150 lb. per sq. in., and may be controlled by an air valve arranged for solenoid or mechanical actuation.

NEW PRODUCTION EQUIPMENT

G. W. Masor and A. J. Barker

Matrix Type TI 1315 Internal Thread Grinder

The Matrix type TI 1315 machine shown in the illustration, has recently been introduced by the Coventry Gauge & Tool Co., Ltd., Fletchamstead Highway, Coventry, for performing internal thread grinding operations on nuts of the ballcirculating type, also nuts and half-nuts with

various thread forms.

Workpieces up to 13 in. diameter can be handled on the machine, and right- and left-hand threads up to 10 in. diameter, with helix angles up to 15 deg., can be ground for a maximum length of 5 in. If required, a special wheel-head can be fitted which enables threads with helix angles up to 10 deg. to be ground for a maximum length of 7 in. Apart from loading and unloading of workpieces, the machine is tully automatic in operation, and can be set for taking a single cut, or a number of cuts up to a maximum of 24 during the cycle. Grinding is carried out with a single-

rib wheel of 3 in. maximum diameter, which is automatically dressed at pre-set intervals. When a number of cuts is to be taken on the work, wheel dressing can be carried out at the beginning or the end of the

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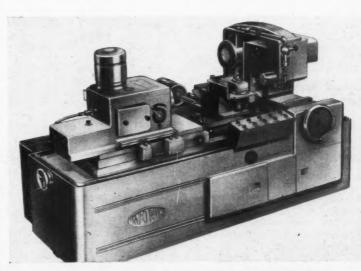
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For grinding nuts of full circular cross section, an increment of infeed is automatically applied to the wheelhead at each reversal of the work-head slide, and the maximum feed movement obtainable is % in. When a half-nut is to be ground, in-feed is applied before the work-spindle is started, for grinding the thread to a pre-set depth at a

single pass. Drive to the spindle is then engaged, and at the end of the grinding stroke, the wheelhead is moved clear, and the spindle is reversed to return the work-head slide to the starting position. When a thread grinding operation has been completed, and for wheel dressing, the wheel-head is withdrawn to its rear-most position by compressed air. Following a dressing operation, the wheel-head is adjusted, the motion again being imparted pneumatically, to compensate for reduction in wheel diameter. The wheel-head and the diamond wheel-dressing attachment can be tilted to each side of the horizontal position for setting to suit the helix angle of the thread to be ground.

Grinding spindle units of two different types are available, one of which is driven by a belt from a 5-h.p. motor, and can be run at speeds of 15,000 and 18,000 r.p.m. The other unit is driven by a high-frequency motor, and the steplessly-variable spindle speeds obtainable range from 12,500 to

40,000 r.p.m.



Matrix type TI 1315 internal thread grinder with guards removed

Drive to the work-head is taken from a 2-speed motor of 1½/3 h.p., and 14 spindle speeds from 6 to 210 r.p.m. are available. From the spindle, drive for traversing the work-head is taken by a lead bar and nut. Interchangeable lead bars and nuts are available to cover various thread pitches, and the same bar and nut are employed for grinding right- and left-hand threads of the same pitch. The work speed is normally the same for the grinding and return travels of the work-head slide. When very low speeds are employed for grinding certain workpieces, however, a spindle speed of 56 r.p.m. can be engaged to give a faster return travel.

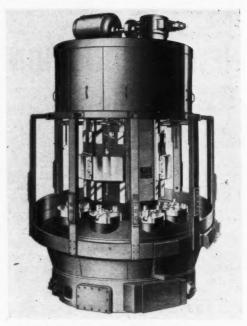
Bored 2 in. diameter, the work-head spindle can be indexed for grinding threads with different numbers of starts from 2 to 6. Adjustment is provided for controlling the ground threads for parallelism, also for bringing pre-machined threads in the work into engagement with the grinding wheel. The work-head slides on a base guideway, which can be adjusted on the bedways to suit the length of the component to be ground. A maximum distance of 151/2 in. can be obtained between the nose end of the work-head spindle and the

Coolant is delivered to the work through the spindle bore, also through separate pipes to the grinding wheel. Another pipe is fitted for delivering coolant to the wheel dressing attachment. A fume extractor system is provided, and the entire working area is normally enclosed by a guard. There is a hinged window in the guard, which can be swung upwards to the open position to give access to the work for loading and unloading.

Rockwell Machine Tool Co., Ltd., Welsh Harp, Edgware Road, London, N.W.2, are the sole selling agents for Matrix thread grinders.

Bullard Type M Mult-Au-Matic Vertical Chucking Lathe

Introduced recently by the Bullard Co., Bridgeport, Conn., U.S.A., for whom the agents in this country are Buck & Hickman, Ltd., Otterspool Way, Watford By-Pass, Watford, Herts., the type M Mult-Au-Matic vertical chucking automatic, here shown, is available with 6, 8, or 12 spindles. the latter arrangement, there are two spindles at each station, to enable two series of machining operations to be performed simultaneously. On the other machines, there is normally one spindle at each position, but equipment can be incorporated for double indexing, if required. A maximum of 17½, 17¼, or 11¼ in. diameter can be swung, depending on the number of spindles, and on the 6-spindle machine, this capacity normally covers a



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Bullard type M Mult-Au-Matic vertical chucking automatic

distance of 8% in. from the noses of the spindles, with provision for swinging 10 in. diameter over a further 6 in. of height. An extended central column can, however, be incorporated, to increase the height capacity for 17½ in. diameter. machine is designed to enable modern cutting tool materials to be used to full advantage, and drive is taken from a motor of a maximum of 60 h.p., through a hydraulically-operated clutch and brake system of new design, wherein compensation is

automatically provided for wear.

The spindle carrier is mounted on a long taper bearing at the lower end of the column, which is secured to a single-piece base casting, and the weight and downward thrust are taken by an adjustable ball bearing. Each spindle runs in three anti-friction bearings, and a total of 41 speeds, from 45 to 400 r.p.m., is obtainable, individually, for each working station, by means of change gears. Two- or three-jaw chucks, of 10, 12, or 15 in. diameter, can be mounted on the 8-in. diameter noses of the spindles, which are of the American standard A-1 form, and may be of the lever- or wrench-operated type. Equipment can be incorporated for power operation of the chucks, with provision for adjusting the gripping pressure.

Feed is applied by a cam system to the tool slides, which are mounted in hardened and ground ways on the column faces, and change gears enable a total of 82 rates, from 0.0024 to 0.1872 in. per rev., to be obtained individually for each of the spindle stations.

A range of heavy-duty tool heads is available, with a maximum working travel of 8 in., and for one unit, which has a single slide, this movement is in the vertical direction only. Single slides are also incorporated in the plain compound and the universal units, and the working travel may be entirely vertical or may include a movement up to 4 in., in either direction horizontally with the former, and in any horizontal or angular direction with the latter.

Two slides are incorporated in the double-purpose unit, one of which provides for a maximum vertical travel of 3 in. The other slide is simultaneously moved horizontally, and feed rates in the ratios 1:1, 4:3, 2:1, and 3:1, also change of direction, can be obtained by interchanging gear brackets, without the need for removing the unit from the machine. Auxiliary heads which can be supplied include single- and multi-spindle drilling and tapping units, also units for internal and external spherical turning.

Coolant equipment can be provided, and the machine, which weighs approximately 11½ tons, occupies a floor space of 8 ft. 4 in. diameter.

18 in. can be accommodated between the centres.

When finishing crowned gears, an oscillating motion is applied, for a maximum angle of 45 deg. on either side of a central position, and with this arrangement, the crown radius is unaffected by the diameter of the grinding wheel. The machine may be operated under manual control, or on a semiautomatic or an automatic cycle, and with the latter, each tooth on the workpiece is rough-ground in a pre-determined number of passes, an increment of down-feed being applied to the wheel-head at each reversal of the work-table. After the completion of grinding at one position, the wheel-head is raised and the workpiece is indexed through one tooth space, in readiness for the sequence to be repeated, and when a pre-selected number of teeth has been ground, the wheel is automatically dressed.

During the dressing operation, an increment of down-feed is applied, to compensate for the amount which is to be removed from the wheel, and the diamond dressing unit is then traversed hydraulically across the face under the control of a template, to produce the required profile shape. Dressing is again performed after the rough grinding stage has been completed, and the teeth are then finish-ground in successive passes, and, finally, the machine is stopped.

Wheels from 3 to 6 in. diameter can be mounted on the grinding head spindle, which runs in preloaded ball bearings and is driven directly by a

Geargrind CGG—16 × 18FA Automatic Grinding Machine for Crowned Gear Couplings

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The CGG -16 × 18FA grinding machine shown in the figure has been introduced recently by the Gear Grinding Division, Michigan Tool Co., Detroit, Mich., U.S.A., and is primarily intended for finishing the teeth on spherical gear-type couplings to a crowned form, although it may be employed for operations on spur gears and splined shafts, also for relieving the ends of teeth of plain spur gears. Numbers of teeth ranging from 3 to 220, of 64 to 4 d.p., can be ground to a maximum crown radius of 12 in. on gears with diameters up to 10 in. over the crests of the teeth and down to % in. at the roots, and the maximum length of cut which can be obtained is 10 in. Up to 17½ in. diameter can be swung, and workpieces which have lengths ranging up to



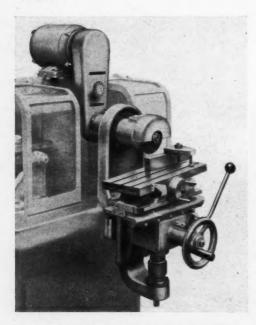
Geargrind CGG—16 × 18FA automatic grinding machine for crowned gears

2-h.p. motor. During grinding, coolant is delivered to the workpiece through the wheel. Vertical movement of the head through a maximum distance of 13½ in. is obtained hydraulically, and the total feed travel can be applied in any predetermined number of steps. The work-table has a maximum traverse of 32 in., and up to 116, 98, and 88 cuts per min. can be taken, when grinding gears with face widths of 2, 3, and 4 in., respectively.

The Michigan Tool Co. are represented in this country by Ex-Cell-O Group Sales, Ltd., Halford House, Charles Street, Leicester.

Beacon Chip-breaker Groove Grinding Attachment

An attachment for grinding chip-breaker grooves in turning tools has recently been introduced for use with the "Superior" type CT 8 grinding and lapping machine for tungsten carbide cutting tools built by Beacon Machine Tools, Ltd., Hurst Lane, Tipton, Staffs. This attachment is shown in the accompanying illustration, and details of the type CT 8 grinder were given in MACHINERY, 93/899—15/10/58.



The new attachment for grinding chip-breaker grooves in turning tools is here shown mounted on the Beacon "Superior" type CT 8 machine

Cutting tools up to 2 in. thick can be handled with the attachment, and the 12- by 6-in. worktable can be tilted through a maximum angle of 5 deg. to the left and right and towards and away from the column which carries the grinding spindle. It has a maximum adjustment of 2 in. on transverse guideways by means of a handwheel, and smooth movements in the longitudinal direction over stroke lengths up to 3 in. are provided by a ballended lever. The knee which carries the table assembly has a vertical adjustment of 2% in. by a large-diameter handwheel through bevel gears and Graduations are provided round the periphery of the handwheel for vertical adjustment, which give readings to 0.00025 in., and the spindles for the bevel gears are fitted with ball thrust bearings, and can be adjusted to eliminate backlash. The traversing screws for the vertical and transverse movements engage with renewable phosphor bronze nuts, and the guideways are fitted with gib pieces to permit adjustment for wear.

Mounted in Timken precision taper roller bearing, the spindle will take a 4-in. diameter by %-in. wide diamond-impregnated grinding wheel, and is driven at a speed of 4,700 r.p.m. by a flat belt from a %-h.p. totally-enclosed motor. The attachment weighs approximately 1% cwt.

New Shore Scleroscope Hardness Testers

The Shore Instrument & Mfg. Co., New York, U.S.A., have recently introduced two new Scleroscope hardness testers known as the types C.2., and D. Stated to be very simple to use, the C.2. Scleroscope is an improved, direct-reading instrument, which is suitable for testing thin metal sheets, for example, of hardened steel from 0.006 in. thick and of cold-rolled, unannealed, brass and steel from 0.015 in. thick. It can also be employed for testing machined parts such as chilled iron and forged steel rolls, gears, and shafts.

An advantage of the instrument, for production purposes, particularly where highly finished surfaces are concerned, is that the diamond hammer leaves no impression visible to the naked eye, even on strip with a mirror finish. The instrument may be used "freehand," so that inspection can be carried out anywhere along a production line, and on components in position on machine tools and presses. Alternatively, it can be mounted on a stand or in a swing arm clamp on a test bench. A conversion table to Brinell and Rockwell C scales is available.

With the type D Scleroscope, which is shown in the accompanying illustration, the hardness number is read by means of a dial and pointer,



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The Shore Model D Scleroscope hardness tester

instead of on a vertical scale behind the hammer tube. The scale is also graduated in Brinell and Rockwell C hardness numbers. This instrument will test all materials for which the type is suitable, but is not recommended for use freehand.

selection of clamping devices is available.

The sole agents for these Shore instruments in

the United Kingdom and the Commonwealth, except Australia, are Griffin & George (Sales), Ltd., Ealing Road, Alperton, Middlesex.

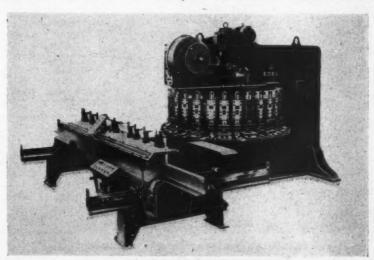
Edel Turret Presses with Co-ordinate Tables

To facilitate the production of workpieces with large numbers of holes, such as the chassis for

electrical equipment, turret presses in the German-built Edel range, which is marketed in the United Kingdom by F. J. Edwards, Ltd., 359-361 Euston Road, N.W.1, London, can now be supplied with co-ordinate setting work-The well-balanced table of each of these units can be traversed from left to right, and vice versa, on a single upper guide rail, and the entire assembly can be moved towards and away from the press on twin lower guides, as shown in the figure. Multiple stop members can be provided to facilitate positioning when repetition work is being performed. Operating controls are conveniently placed at the front of the unit.

Edel turret presses can also be equipped with template tables and other positioning arrangements, and are available with capacities up to 100 tons, throat depths up to 31 in., and numbers of punching stations between 12 and 40. If desired, alterations can be made to the standard design, to suit individual requirements. The turret of each machine can be indexed in either direction, and after completion of the movement, is located accurately and locked by means of a slide, which is traversed along ways on the housing, to bring a groove into engagement with the stop for the working station. This slide is normally operated by means of a lever, but a solenoid can be provided, if required, to enable it to be controlled from the co-ordinate table. On machines up to 35 tons capacity, turret indexing is effected manually, and a telescopic arm can be provided to facilitate the operation. The turret of a machine with a capacity of 50 tons or more is turned by power, under push-button control, and the transmission system incorporates a slipping arrangement, to ensure that no damage is caused if the locking slide is engaged before drive is released.

The press tool at the working station is operated by a hardened and ground ram, which is mounted in long, adjustable ways on the upper part of the fabricated steel frame. Motion is transmitted to this ram by an eccentric shaft, which runs in



Edel turret press, with co-ordinate setting work-table

special bronze bearings, and drive is taken from a star-delta motor to a balanced flywheel, and thence through roller bearing-mounted shafts and totally-enclosed reduction gearing. A hardened and ground, multi-tooth dog clutch is incorporated in the transmission. To facilitate setting, the ram may be adjusted vertically by means of a handwheel.

Fan-type Unit Drilling Heads

To facilitate drilling and tapping holes in the gimbal ring for the Hawk missile, Edlund Machinery Co., Cortland, N.Y., U.S.A., have supplied to the Missile Systems Division of the Raytheon Co. three special-purpose machines which are equipped with unit drilling heads built by the United States Drill Head Co., Cincinnati, Ohio, U.S.A. These heads are of the company's standard and fan types, and examples of the latter are seen in the accompanying close-up view.

The super-finished multiple drilling spindles of each of these heads are mutually inclined, at various total angles up to 90 deg., and are mounted in a housing attached to the machine base. Feed movement is obtained by traversing the spindles axially through the housing, and for this purpose, the rear ends are connected to a pusher plate, which is guided by cylindrical bars that project from the housing. The movement is applied by

from the housing. The movement is applied by means of a cam-operated Edlund unit, the flanged from 0.01

Mounted on a special-purpose Edlund machine, these fan-type multi-spindle drilling heads, made by the United States Drill Head Co., provide for machining mutually inclined holes

quill of which is secured to the plate. Drive for the head is also taken from this unit, by a shaft which extends through the pusher plate, and is transmitted to the spindles, some of which are rotated at speeds in excess of 2,500 r.p.m., by special gearing in the housing. Shaved gears are employed, and the splined shafts on which they are carried—also the drilling spindles—run in ball bearings.

Fan-type heads can be built to suit a wide variety of requirements where the individual hole axes are not parallel. Mounting arrangements can be provided to suit individual applications, to permit easy installation and removal. The heads may be mounted horizontally or vertically, also on standard drilling machines, and it is stated that the open design affords ready access to the spindle chucks for tool changing, and enables drilling and tapping to be carried out at successive stages with the same unit.

DOHMPOWDER NYLON POWDER. The Plastics Division of Dohm, Ltd., 167 Victoria Street, London, S.W.1, has introduced Dohmpowder type 6 nylon powder which is suitable for dip or flame spray coating. The corrosion resistance of this powder is stated to be very satisfactory except against mineral acids, and it has an electrical resistance of 600 volts per 0.001 in. thickness of coat. Deposit thickness obtainable by dip coating ranges from 0.010 in. to 0.025 in., and by flame spraying,

from 0.010 in. to virtually any economical value. The working temperature range is from -40 to +140 deg. C., and the approximate melting point is 190 deg. C. Coatings have a relatively high impact strength and are claimed to be particularly suitable for application to metal and glass. Dip coating is most suitable for articles produced in light industry, for example, electrical goods and metal window frames. Flame spraying, it is suggested, could be employed for coating car and commercial vehicle bodies, storage tanks, and other parts too large to permit dipping to be carried out.

THE PRODUCTION OF FORK-LIFT TRUCKS in the first quarter of this year rose to 1,679, compared with 1,210 for the same period of 1960. Total values of all types of powered industrial trucks delivered in these periods were £2,523,000 (1960) and £3,406,000 (1961).

Improved Facilities for Continuous Casting of Encon Copper-base Bearing Alloys

THE WORKS OF ENFIELD ROLLING MILLS, LTD., Brimsdown, Enfield, Middlesex, have recently been extended, and additional equipment has been installed, which has enabled the production of Encon continuous cast rods, tubes, and bars of special cross section, to be doubled. New stores and despatch departments have been provided, to give improved facilities for the distribution of stock products in this range, which now includes more than 1,500 items, to customer firms and to the company's depots in various parts of the country.

Continuous cast rods, tubes and bars can be produced in phosphor bronzes, leaded phosphor bronzes, gunmetals, and leaded gunmetals, to the B.S. 1400 specifications, and to others if required. Solid bar is made with diameters from $\frac{7}{16}$ to $\frac{7}{16}$ in., and tubes with outside diameters from $\frac{7}{25}$ to $\frac{7}{16}$ in., and bores down to $\frac{15}{25}$ in. Dimensional limits for bars and the outside diameters of tubes are +0.004 -0.006 in., and the concentricity of the bore with the outside diameter of a tube is held within $\frac{1}{2}$ per cent of the wall thickness. Bars are normally

supplied in lengths up to 12 ft., but longer hars can be provided if required. All bars produced in the plant are mechanically straightened, so that the arc depth in any 5 ft. length does not exceed ¼ in.

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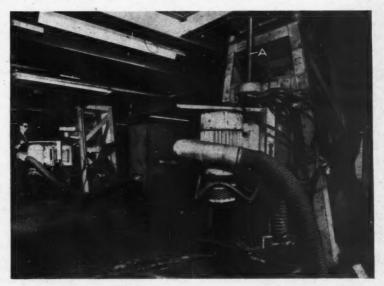
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The procedure for the production of Encon bars was described in some detail MACHINERY, 90 / 417-22/2/57, and it will be recalled that two Birlec-Detroit 500-lb. capacity rocking arc melting furnaces, and associated continuous casting plants, were then employed. A third Birlec-Detroit furnace, with the necessary casting plant, has now been installed, and provision has been made for a fourth to be brought into operation in the future. The continuous casting plant is similar to that developed by the American Smelting & Refining Co., New Jersey, U.S.A., and is operated under licence from that company.

Constituents of the alloy to be melted are weighed into a wheeled skip, which is then raised to the top floor of the 4-storey building. Here, the constituents are discharged from the skip into one of the melting furnaces. When the melt is ready, the furnace is tilted hydraulically for transferring the molten metal into the charging box of the adjacent casting furnace, which is lined with refractory, and is heated by carbon resistors. supply of nitrogen is maintained in the furnace to provide an inert atmosphere to prevent oxidation of the metal. At the beginning of the casting operation, a starter bar is inserted in the watercooled graphite die which is mounted at the lower end of the furnace. When the shut-off plug has been opened by means of a handle on the casting floor below the furnace, molten metal enters the die and freezes on to the starter bar. The latter is



In this view are shown two flying cut-off machines installed at the works of Enfield Rolling Mills, Ltd., for cutting pieces of required lengths from continuous cast bar

then drawn downwards by a roll mechanism installed on the casting floor. When the metal emerges from the die, it has cooled sufficiently to support the molten mass above, and casting continues as long as the cooled metal is withdrawn from the die at a constant speed. The starter bar is removed when the cast bar or tube emerges from the rolls.

The bar then passes through a hole in the casting floor to the next level in the building, where it is cut into the required lengths by a resinoid-bonded abrasive wheel mounted on the motor-driven spindle of a flying cut-off machine. Two cut-off machines, associated with separate casting plants, may be seen in the figure, and part of a continuous bar is indicated at A. The counter-balanced cut-off machine is secured to the cast bar by means of a clamp, so that it travels with the bar for the cutting operation, and is guided by means of rollers, which engage with the faces of a vertical

steel column of hexagonal cross section. The piece cut-off from the bar is received by a tube on the ground floor of the building. This tube, which is pivoted, is then swung downwards to discharge the piece on to a horizontal run-out table, where it is inspected and then passed to the straightening machine.

Very little wear on the die takes place during casting, and it is stated that a single die may be maintained in continuous operation for a period exceeding 100 hours, and that the amount of metal cast per hour may range from 100 to 800 lb. Since, however, a new die is employed at each set up, the average working life is about six hours. Dies for continuous casting are made in a separate shop at the Brimsdown works. In addition, a well-equipped machine shop has been provided for the production of components such as bushes, bearings, washers and valve guides from Encon continuous cast bar, on a contract basis for customer firms.

Transfer Mechanism for Cylindrical Workpieces

By L. KASPER

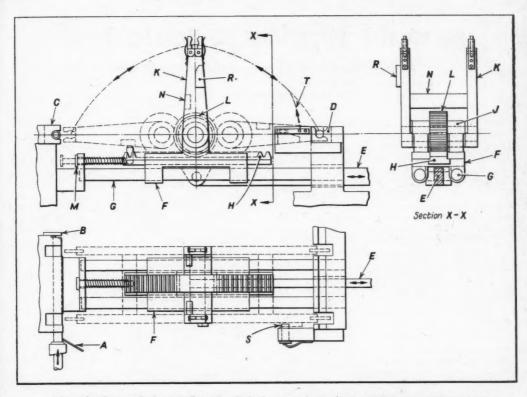
AN ARRANGEMENT FOR TRANSFERRING cylindrical workpieces from one work station to another is shown in three views in the accompanying figure. The mechanism was developed specifically for removing cut-off lengths of tubing from a sawing machine and delivering them to an adjacent work station, but it can readily be adapted for other types of workpieces. Shown diagrammatically at the left in the plan view, the saw A is set to sever the tube at an angle to the longitudinal centre line. The tube is fed in the direction of the arrow by a grip-and-release collet arrangement, advances it to the stop B. As it is advanced, the tube is thrust into the throats of two members C, and subsequently the transfer mechanism provides for withdrawing the cut-off length from these members, swinging it up and over through 180 deg., and depositing it in two further slotted The tube is subsequently ejected members D. from these members by a plunger-type device, not shown.

In the figure, the mechanism is seen at the midpoint of its travel, and the prime mover is the rectangular-section bar E, which is reciprocated longitudinally by a cam (not shown). One end of this bar is attached to a block F, which is arranged to slide on cylindrical guide bars G. In the upper surface of this block there is a central channel, in which the rack H is free to slide, and projecting from the block at either side of this channel there

are bearing bosses J. A shaft passes through these bosses and to each end of it is keyed an arm, as at K, the two being accurately aligned with each other. Keyed to the centre of the shaft, and guided between the inside faces of the bosses J, is a pinion L, which is in mesh with the rack H.

Projecting from the left-hand end of the rack H is a headed stud M, which passes through a guide block, and the compression spring seen on the stud continually urges the rack to the right. Starting from the mid-travel position seen in the side view, and assuming that the bar E is moving to the left, the pinion L is rolled along the rack (which is held stationary by the compression spring) and the arms K turn in an anti-clockwise direction. This movement is arrested when the plate N, which bridges the two arms, makes contact with a stud P, projecting from the teeth of the rack.

Since the arms can no longer turn, the rack H and the block F move to the left as one unit, partially closing the compression spring, and the spring-loaded fingers at the ends of the arms K are thrust over the tube in the members C. The cam which moves the bar E has a dwell portion, which retains the mechanism in this position while the saw A advances to sever the tube. Subsequently, the cam starts to return the bar E to the right, and for the first part of this movement the block F and the rack H travel as one unit, the rack being moved by the compression spring. During this stage, the



Mechanism for transferring cut-off lengths of tube from a sawing station to an adjacent machining position

arms do not move angularly, and the tube is withdrawn from its seatings. Immediately the head on the stud M abuts the associated guide block, however, movement of the rack is arrested. The block F continues to move to the right, and the pinion L starts to roll along the rack, the arms being thus turned in a clockwise direction until ultimately the tube is deposited in the slots in the members D

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During the final stage of the angular movement of the arms, a projection R passes the springloaded latch S, which is thus thrust back into its housing. Immediately the projection is below the latch, the latter advances again to the position shown. The bar E is now moved to the left once more, and in the early stages of travel, angular movement of the arms K is prevented by the engagement of the projection R with the underside of the plunger S. As a result, the block F and the rack H again move as a complete unit, against the action of the rack spring, and the arm fingers

are pulled from the tube, which remains in the members D.

Immediately the projection R is clear of the plunger S, the arms are free to move angularly, and initially such movement occurs fairly rapidly, since the rack H is moved quickly to the right when the compression spring re-asserts itself. The path of the arm fingers during the early stages of the return movement is shown by the dotted curve T. Excessive angular acceleration during this period is prevented by providing a suitable cam surface on the projection R, to ensure that it disengages gradually from the latch S.

PEDAL CYCLES delivered during April of this year totalled 208,000, which was 4,000 more than the figure for the same month in 1960. Cycles exported in April, 1961, reached a total of 148,000, and this figure was 2,000 more than the highest monthly total for the previous year.

Automatic Detection of Broken Tools

Some Methods Employed on High-production Machine Tools

By KARL-HEINZ WOLFRAM, Dipl. Ing.

WITH THE INCREASING USE of fully-automatic highproduction installations, such as transfer machines and link-lines, the importance of providing means whereby tools are continuously monitored during operation has become more apparent. If costly and time-consuming interruptions to production are to be avoided, or reduced to the minimum, it is essential that broken tools-notably drills, taps, reamers and counterbores-should be detected and that the required action should be taken immediately. Extensive damage can result, for example, if a tapping-size drill breaks in a workpiece and the latter is then automatically transferred to a tapping station. If a signal can be transmitted at the moment of breakage-or at least before the next machining cycle has been started—it can be ensured that only one tool and one workpiece are affected.

One of the most common methods of continu-

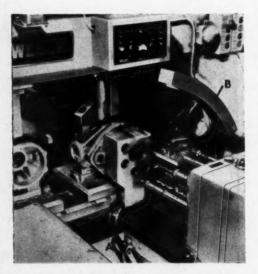


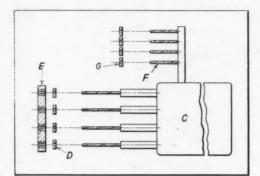
Fig. 1. A photo-electric arrangement whereby the tools in a multi-spindle head are continuously monitored for breakage by means of a number of light rays converging on a single receiver cell

ously checking drills and taps, or the holes that they produce, is by the provision of specially-designed probes. These units can be applied in two ways, namely, by introducing a probe into the hole, or by advancing a probe towards the tool, after the latter has been withdrawn from the work. It will be appreciated that if the hole is faulty, or contains part of a broken drill, the probe cannot complete its full stroke, and a simple switching system can be arranged to interrupt the automatic cycle and operate an audible or visual alarm. A similar arrangement can be provided in connection with a tool-probing mechanism.

With these methods, time must be allowed during the machine cycle for the probing operation to take place, and the mechanism must provide for swinging the probe clear of the tool-path before the next cycle is started. From these standpoints, certain advantages are offered by photo-electric monitoring systems, since they can invariably be mounted permanently clear of the working zone, and extra time need not be allowed in the automatic cycle for their operation. An example of a photoelectric monitoring arrangement for a multi-drilling head is shown in Fig. 1. The receiving cell is indicated at A and is arranged to be at the focal point of a number of lamps in the arcuate container B. The lamps and receiver are on opposite sides of the battery of drills and it is arranged that at all positions of travel of the multi-spindle head each of the rays from the lamps in the housing B is obstructed by one of the tools.

If a tool should break, however, light from the associated lamp will fall on the receiver A, and an electric circuit will be completed to stop the machine and energize a suitable alarm signal. It will be appreciated that if the tip of a drill is broken the monitoring system will operate only when the spindle head is in the fully withdrawn position. With such an arrangement, care must be taken to prevent swarf and other foreign matter from collecting on the receiver A, which would have the effect of obscuring the cell artificially, and of preventing the system from operating.

Broken or damaged tools can also be detected electrically, by measuring the inductance of a drill, for example, before and after an operation. With



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Fig. 2. Diagram showing an arrangement of "balanced" pairs of inductance coils for monitoring drills in a multi-spindle head

one such arrangement a coil is mounted adjacent to a guide bush tor a drill. As the drill is advanced towards the bush it first passes through the bore of the coil, and a cam on the spindle head is set to operate a switch whereby the coil is energized when the point of the drill has just passed the inner end of the coil, but has not yet entered the guide bush. In these circumstances, the drill extends for the full length of the coil, and a high inductance is obtained.

Assume, however, that as a result of a subsequent operation, the point of the drill is broken. Under automatic control, the spindle head is withdrawn fully and is then advanced for the next cycle. When the cam-operated switch energizes the coil on this occasion, however, there is a shorter length of drill within the bore of the coil—since the point is broken—and a lower inductance is obtained. This reduction in value can be utilized to operate a relay, for example, to stop the machine and initiate an alarm system. With the inductance method, damage affecting the length of a drill by as little as 0.020 in. can be detected.

For some applications, however, it may not be practical or convenient to employ cam-operated switches for energizing the inductance coils. For deep-hole drilling, with step feed and rapid withdrawal of drills for swarf clearance followed by rapid approach, it may be preferable to employ the arrangement shown diagrammatically in Fig. 2. This system is based on the principle of comparing the inductances from associated pairs of coils, which are arranged to be in "balance" under normal working conditions. At C in Fig. 2 is shown a 4-spindle head, and the inductance coils and guide bush plate are indicated at D and E respectively.

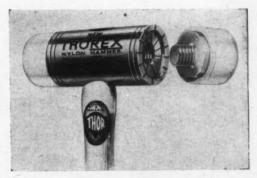
Attached to the spindle head there is a group of dummy tools, as at F, which are of the same diameter and length as those in the main head. Inductance coils G are also provided for these dummy tools and are connected by way of "balancing" circuits to the corresponding coils at D. It will be appreciated that the breakage of any tool in the main head will result in a change of inductance in its associated coil in the group D. Consequently, this change in inductance will upset the balance which normally exists with the corresponding coil in the group G, and the electrical circuit can be arranged to stop the automatic cycle.

Inductance monitoring equipment of the type here described is produced by A. Klenk, Ludwigsburg/Württ., Germany.

New Thorex Nylon-faced Hammer

The Thor Hammer Co., Highlands Road, Shirley, Birmingham, have introduced, as an addition to their range, a hammer provided with renewable faces of Nylon, as depicted in the accompanying illustration. The steel head is internally-threaded and recessed at both ends to receive the Nylon face-pieces, which are shouldered to provide additional resistance to shearing of the threads when angular blows are struck. Radial grooves cut in the end surfaces of the steel head are stated to afford a safeguard against loosening of the Nylon face-pieces in service, but do not prevent them from being unscrewed by hand, to facilitate replacement when worn.

New Thorex Nylon-faced hammers are at present made in a range of five sizes with renewable faces from 1 in. to 2 in. diameter, and with weights from ½ lb. to 3 lb.



The New Thorex hammer is provided with renewable Nylon faces

Diaphragm Chucking

By W. D. BARNETT*

WITH THE INCREASING need for accurate work-holding devices to keep pace with developments in machine tools, the diaphragm chuck has received much attention during the past few years. Although the principle has been known for a long time, it is only comparatively recently that such chucks have been developed to provide for highly-accurate holding, as now required.

The principle of operation involves the deformation of a flat metal diaphragm by mechanical, hydraulic or pneumatic means, the stored energy then being used to grip the work when the pressure on the diaphragm is released. Fig. 1 gives a sectional view of a typical chuck of this type. The diaphragm A is distorted outwards by the pusher sleeve C when pressure is applied to the piston B. The work is then inserted between the jaws, and when the air or hydraulic pressure behind the piston is released, the diaphragm tries to resume its normal shape, and the jaws close.

to resume its normal shape, and the jaws close.

As indicated in Fig. 2, the jaws do not remain parallel as they open, and they therefore require

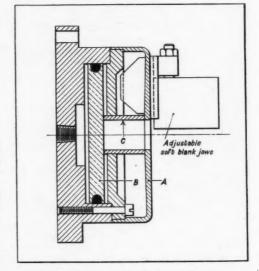


Fig. 1. A typical diaphragm chuck

to be ground accurately to size at the gripping diameter, with the diaphragm under pressure. Grinding is stopped when the work is a tight push fit in the jaws, and it is then only necessary to increase the air or hydraulic pressure slightly to allow the work to be inserted easily. Certain restrictions must be borne in mind in considering whether diaphragm chucking is suitable for a particular workpiece. In the first place, the jaws

have only a limited movement, and the part to be held must have a machined surface where the jaws grip. The more accurate this gripping surface, the more accurate will be the final machining operation. However, the diaphragm chuck will normally tolerate a variation up to ±0.0025 in., and still give satisfactory results.

The second restriction is the gripping force available, the maximum force exerted by a diaphragm depending upon its size. As a guide it may be noted that a 5-in. diameter chuck will exert a force up to 1,100 lb., a

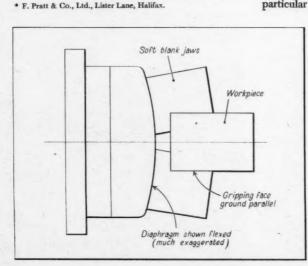


Fig. 2. Diagram showing, much exaggerated, the effect of flexure of the diaphragm

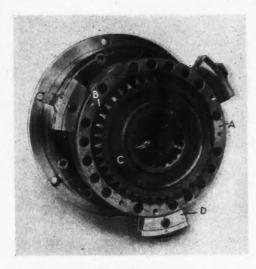


Fig. 3. Pitch-pin diaphragm chuck with interchangeable cages for different gears

7 in. chuck, up to 1,900 lb., and a 10 in. chuck, up to 4,000 lb. Where a gripping force lower than maximum is required, for instance, to prevent distortion of thin-wall components, the jaws are ground out at a lower applied pressure.

Diaphragm chucks are constructed either with or without end stops between the jaws and at the centre, end stops being very desirable when a component must be machined accurately to length. The diaphragm, by the nature of its grip, tends to pull the component back against the stops during the closing action, thus ensuring accuracy of

location. It is therefore preferable to make use of this feature where possible, rather than rely on steps in the gripping jaws for endwise location.

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usually employed for quantity production and is often designed for one particular component. This applies, for example, to pitch-line gear chucking, where the pitch pins are brazed to the diaphragm in positions to suit the gear, since the number of teeth is not always equally divisible by the number of pins. Often a chuck can be made to hold a number of different gears when the quantities do not justify the provision of a chuck for each design. For this purpose, an interchangeable cage may be provided for the pitch pins, as illustrated in Fig. 3. The cage A is held in position by three screws in the end stop locators, and the three ball-ended pitch pins B, which engage the teeth of the workpiece C, are a sliding fit in radial holes in the cage. The gripping pressure is applied to the pins by three equally-spaced diaphragm jaws D. With this arrangement, it is necessary to provide only a cage for each size of gear, and the cage is easily changed by removing three screws.

Diaphragm chucking is of particular advantage when high accuracy and light gripping are required, as in grinding and fine boring. The required, as in grinding and fine boring. method can, however, be sometimes adopted where extreme accuracy must be combined with heavier As an example, it was required to cut internal helical gear teeth in a ring component, on a Drummond Maxicut 2A vertical gear shaper. A special diaphragm chuck, shown in Fig. 4, was employed to withstand the very heavy torque The chuck is of generally conventional design, with brazed-on jaws to suit the component, but attached to the diaphragm is a drawbar which passes through the machine spindle and is connected to an air cylinder. By selecting the right size of cylinder, any desired gripping force can be obtained, while retaining all the features of a normal diaphragm chuck.

If a component is too long for the jaws of a

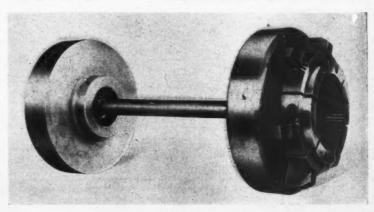


Fig. 4. Special diaphragm chuck for gripping rings in which internal helical gear teeth are to be cut

conventional chuck, it may be possible to employ a double diaphragm chuck to provide for gripping at both ends. Again, a chuck can be so designed that a long shank on a workpiece is accommodated in the machine spindle, and supported by a centre. Although diaphragm chucking has been employed to solve numerous problems, it appears that its potentialities are by no means fully appreciated. It is strongly recommended, however, that anyone contemplating the adoption of this method of work-holding should consult one of the specialist companies at an early stage.

Producing Accurate Eccentric Shafts and Housings

By W. SHARP

A batch of eight eccentric shafts and mating eccentric housings, as shown at A and B, Fig. 1, was required to be produced, with the offset on the shafts within 0.0002 in. of that of the housings. Location of the parallel portions of the components in fixtures would not have guaranteed the accuracy required, and it was decided therefore, to provide for location from taper surfaces.

The housing B was finish machined all over except for the 4.3311/4.3297 in. eccentric bore, which was roughed out on a drilling machine to approximately the required offset. Next, the taper

portion was accurately ground to fit a special mild steel locating sleeve seen at x in Fig. 2. For finish boring the $4\cdot3311/4\cdot3297$ -in. eccentric diameter, the taper portion of the workpiece was inserted into the locating sleeve, and the latter, in turn, was located in the spindle nose of a Swift 12V6 centre lathe. For clamping, a plate was applied to the front of the workpiece, and pulled back by studs which were passed through the holes in the spindle nose.

Initially, the eccentric shaft was turned and ground concentric along its entire length, the

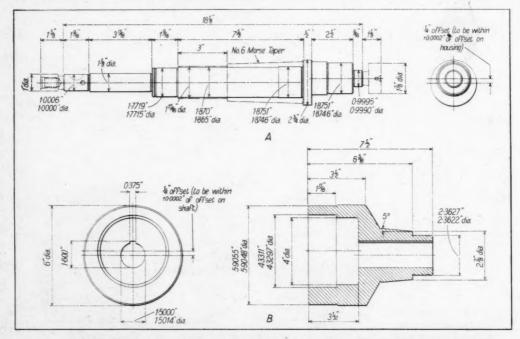
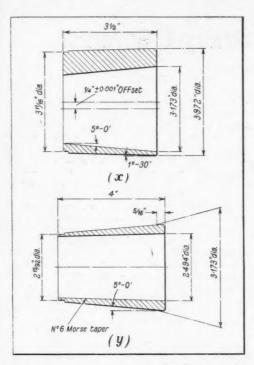


Fig. 1. A shaft component A and a mating sleeve B which were required to be machined to an accuracy of 0.0002 in. for eccentricity.



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Fig. 2. Locating sleeves employed for the eccentric boring and turning operations

portions shown chain dotted in Fig. 1, being provided for manufacturing purposes. These extra

portions comprise an extension at the left-hand end, with a tapped hole to receive a draw bar, a right-hand extension to take a centre hole which otherwise would have come too close to the outside of the smallest eccentric diameter, and a section of No. 6 Morse taper near the centre, for location purposes.

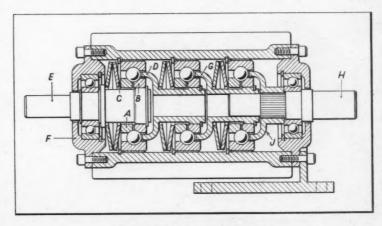
For turning the eccentric portions of the shaft, the Morse taper was inserted in the sleeve shown at y in Fig. 2, which, in turn, was located in the sleeve x already in the spindle

nose of the lathe, the shaft being held by a drawbolt in the tapped hole. When the eccentric portions had been finished, the end extensions and taper section near the shaft centre were removed.

Angus Ball Drive Units

Reference was made in Machinery, 98/1028—3/5/61, to the ball drive units, of patented design, which have been introduced by George Angus & Co., Ltd., Gear Division, Hebburn-on-Tyne. In these units, rolling bearings are employed as epicyclic reduction gears to provide a friction drive, and a typical arrangement is shown in the accompanying drawing. The actual speed reduction between the inner race and the cage depends on the relative diameters of the balls and the tracks of the inner and outer races. For bearings of normal proportions, each reduction ratio approximates to 2.4 to 1 and 3.2 to 1,

For this design of reduction gear, ball or taper roller bearings can be used, but radial ball bearings are preferred. Inner races of the bearings in the unit shown, are split circumferentially, as indicated at A and B, and the friction drive is obtained by applying axial pressure through the medium of spring-steel dished washers C. The ball cage, as at D, forms the mounting spigot for the inner race of the following bearing, and the total reduction obtained depends upon the number of bearings coupled in series. A ball bearing in the end cover F supports the input shaft E, and the second ball cage G runs on an extension of the output shaft Splines in the cage *J*, of the last bearing, transmit the drive to the output shaft. The unit is filled with oil, and there are cooling fins on the casing.



Angus ball drive speed reduction unit

A Quick-acting Centrifugal Governor

By J. BOAS POPPER

A STEAM TURBINE installed in a chemical plant was required to operate up to a certain rotational speed, and the use of a conventional centrifugal governor was not acceptable, as it was essential to provide some device that would be virtually instantaneous in operation. As a result, the quickacting centrifugal governor shown in Fig. 1 was developed, which is unorthodox in design and has proved very effective. In operation, the unit is rotated about its longitudinal centre line, and in Fig. 1 is shown in what may be termed the "closed" position. The various moving parts are in the positions illustrated when the governor is stationary, also when it is approaching—and is very close to-the maximum allowable speed. In these conditions, the small diameter plunger A projects only slightly from the body of the unit. When the required speed is reached, however, the moving parts rapidly change positions, and as a result the plunger A is extended, this axial movement being employed to regulate the steam supply to the turbine.

The principle on which the governor operates is shown diagrammatically in Fig. 2. A shaft B is carried in bearings and is driven directly from the turbine, or indirectly at a proportional speed. At one end of the shaft B there is an arm C, which is pivoted at its centre point and can oscillate through a limited angle, about an axis which is at rightangles to the longitudinal centre line of the shaft B. Also attached to the shaft B, and arranged to rotate with it, is an arm D which serves as an anchor point for one end of a tension spring. The other end of this spring is attached to the arm C, and serves to bias the arm in an anti-clockwise direction, to hold it in contact with the limiting stop E. This stop, also that indicated at F, is attached to, and rotates with, the shaft B.

It will be appreciated that as the speed of the shaft B increases, a point will be reached at which centrifugal force exerted by the weights on the arm C is greater than the restraining force of the tension spring. The arm C will then move rapidly in a clockwise direction, to take up the position shown by the dotted line in Fig. 2, and this movement can be converted to linear motion and utilized to control a servo-system. It should be mentioned that the anchor bracket for the tension spring must be movable axially in relation to the shaft B, so that when the arm C is in the dotted position the spring is still at right angles to the shaft B. Immediately the rotational speed falls, and likewise the centrifugal force acting on the arm C, the tension spring takes charge and the

mechanism is rapidly returned to its

original setting.

Three sectional views through the unit shown in Fig. 1 are given in Fig. 2, and reference will first be made to the view at X. It should be noted that in this view the governor is shown in the "open" position, the centrifugal force having overcome the spring, so that the plunger A is extended. There are two weights, one of which is indicated at G, and these weights are arranged opposite to each other and are pivoted at their centre points. The weights G are similarly lettered in the section Z-Z and Y-Y, where the pivot bearings, which are of the needle type, are indicated at J. These weights are of brass, and are "crossed," the other weight, not shown in the view X, being arranged with its longitudinal centre line inclined in the opposite direction.



Fig. 1. General view of a new quick-acting centrifugal governor, designed to control a steam turbine

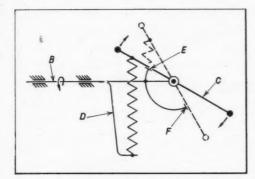


Fig. 2. The principle of operation of the governor is here shown in diagrammatic form

At the centre of each weight there is a steel portion, as at H, which has an irregularly-shaped projection, indicated at K. These projections "overlap" each other, and when the governor is in the open position they abut at the point L, to

limit the turning movement of the weights. In the closed position, the projections L abut at the points M. It should be mentioned that in the view at X both the projections K are shown, for purposes of explanation, although that shown shaded would not actually be visible in the plane of section.

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In the practical application, the tension spring shown in Fig. 2 is replaced by the C-spring N, which is indicated in all three views of Fig. 3, also in Fig. 1. It will be seen that this spring tapers to a point at each end, and is widest at the middle, since with this design linear force characteristics can be combined with a large allowable deformation. Moreover, with a spring of this type, a line joining the ends will always be perpendicular to the centre line of the unit, which is a geometrical requirement of the design. The ends of the spring are secured in small holes in the edges of the projections K, and the tendency is for the spring to turn the weights about their respective axes and to bring the points M, on the irregularly-shaped projections, into abutment.

Projecting from one face of each weight G there is a small-diameter pin, as at P, which engages with a sheet-metal sliding member R (all views in Fig. 3). These sheet metal members are joined at one end by a bridge piece S, also indicated in Fig. 1, and this member, in turn, is secured to the plunger A. As the weights turn, the pins act in slots in the members R and move the latter in a direction parallel to the centre line of the unit, to extend the plunger A.

It will be appreciated that in service there is a strong centrifugal force acting along the axes of the bearings J, as the moving parts of the unit endeavour to spread. To accommodate this force, hardened steel end covers, as at T, are provided, which are secured to the body of the unit by means of screws.

In the application for which this governor was

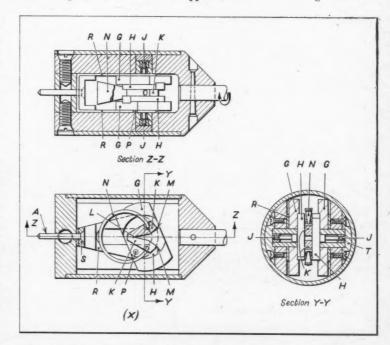


Fig. 3. Three sectional views of the governor, showing the practical application of the theoretical design in Fig. 2

designed, there was no necessity to provide for adjustment to suit various critical speeds. Such a facility can readily be afforded, however, by arranging for the effective radial distance of the weights to be adjustable relative to the pivot bearings I.

Governors of this type are produced by Moked, Haifa, Israel.

Rotary-cutter Attachment for a Lathe

By JOSEPH A. CIVITARESE

It was required to machine a number of annular grooves in the periphery of a cylindrical housing, for cooling purposes, as shown in Fig. 1, and for this operation the special lathe attachment seen in Fig. 2 was designed and made. The base A takes the place of the normal tool-post of the machine and at its centre there is a large-diameter tapped hole. Into this hole is screwed the shouldered post B, which has two portions of different diameters, ground accurately concentric. Arranged to turn freely on this post there is a sleeve C, with a large-diameter portion at its lower end, on the periphery of which plain spur gear teeth are cut.

At the top of the sleeve, there is a reduced-diameter portion which is threaded to receive the cutter D and a lock-nut to secure the latter in position. The sleeve C is retained on the post B by a washer, stud, and lock-nuts. Enclosing the toothed portion of the sleeve C there is a rectangular cover member E, which is bolted to the base A and serves to guide the rack F. This rack is supported at the required height above the lathe bed,

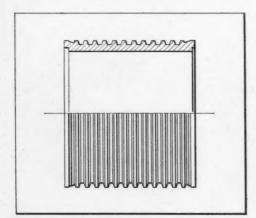


Fig. 1. The annular cooling fins on the periphery of this hollow cylindrical housing were machined on a lathe with the special rotary tool-post shown in Fig. 2

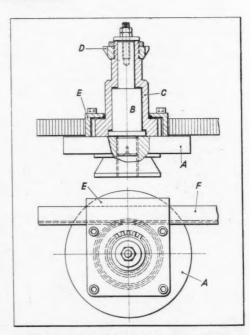


Fig. 2. Sectional and plan views of a special toolpost for use on a standard lathe. A disc-type toothed cutter is employed, and is rolled in "mesh" with the work to produce annular grooves

and accurately parallel to the latter, by special brackets secured adjacent to the headstock and tailstock.

The rack is held stationary, and when the saddle is traversed longitudinally, as for conventional turning, the sleeve C and the cutter D rotate, as a result of the engagement of the teeth with the rack. An O-ring in the cover E forms a seal with the centre portion of the sleeve C, to exclude dirt and swarf from the meshing area of the rack E. With this arrangement, the cutter teeth "mesh" with the workpiece, and machine the annular grooves shown

in Fig. 1. Provision is made, in the brackets which support the rack, for adjusting the latter transversely, between cuts, so that the tool-post can be fed forward to the required depth, also for setting the equipment in order to suit workpieces of different diameters.

The device can also be applied to facing operations, by mounting the rack at right-angles to the bed-ways, and with this arrangement a series of concentric grooves can be machined in a workpiece.

Moreover, for conventional turning work, a plain

disc-type cutter can be substituted for the toothed cutter D. For this application, the cover member E is turned through 180 deg., to bring the rack into mesh with the opposite side of the sleeve C, to reverse the rotation of the latter so that the cutter turns "against" the direction of feed motion of the saddle.

Advantages gained from this method of turning include increased tool life, since wear is distributed over a greater length of cutting edge than is presented by a conventional tool, and the elimination of thread-type feed marks.

Radiovisor No. 27B-R Robotron Die-Saver

Known as the No. 27B-R Robotron Die-Saver, the equipment shown in the accompanying illustration has been introduced by Radiovisor Parent, Ltd., Stanhope Works, High Path, London, S.W.19, and is intended to prevent damage due to the incomplete ejection of parts from the tools on power presses. It is suitable for use on machines which are electrically controlled, or can be modified to provide for electrical operation of the clutches.

Housed in a steel case measuring 13 by 10 by 7% in. internally, the control unit may be attached to the frame of the press, and incorporates a relay, which is energized initially by the electrical signal transmitted when the capacitance of an oscillator coil, mounted in a remote detector head,

is altered as a completed workpiece moves past it. In this way, a set of normally-open contacts is closed, to permit the press to start a fresh operating cycle. The relay remains energized, under the control of an electronic timer, for a period which may be pre-set to correspond to the time which elapses between the production of successive components.

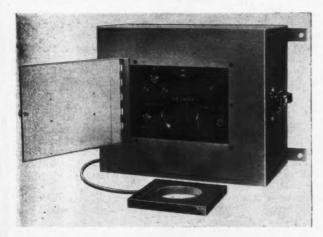
With this arrangement, the normally-open contacts are maintained in the closed position so long as signals are received at the correct intervals, and operation of the machine is permitted to continue. In the event of a component not being ejected past the detector, however, the contacts open, and the next cycle cannot be started. Provision is made for adjusting the sensitivity, to

suit the size of the workpiece, and the unit will normally operate at rates up to 180 impulses per min.

A range of standard detector heads is available, and the type A seen in the figure can be supplied with a central opening of I, 2, 3, or 6 in. diameter, and in thicknesses ranging up to 1 in. Parts may be passed through this opening, or the head may be mounted either above or below the ejection path. The type P head is intended for use where space is limited, or when it is required to provide for detection close to the tool, and measures % in. diameter by 6% in. long.

measures % in. diameter by 6% in. long.

INDUSTRIAL BUILDING IN GREAT BRITAIN. In the first quarter of 1961, approval was granted for the erection of a total of 548 industrial buildings in Great Britain, representing a floor area of 15,997,000 sq. ft.



The Radiovisor No. 27B-R Robotron Die-Saver control unit for use on power presses, incorporates a remote head for detecting the ejection of workpieces

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Reaction of the German Machine Tool Makers to the Melman Report

By A CORRESPONDENT

THE MELMAN REPORT, which has been the subject of considerable criticism in this country, has provoked similar reactions in Germany, where the Machine Tool Makers' Association (V.D.W.) commissioned Dr. F. Eisele, of the Technical High School, Munich (himself a machine tool builder for twenty years), to examine the report. His conclusions, which are presented in a survey extending to some 9,000 words, are here summarized.

Any demand for a technical and economic assessment of a branch of industry which presents such remarkable differences between East and West as does the machine tool industry should be based on the most thorough enquiries. There are, in Europe, more than 1,700 machine tool makers, employing between 10 and 3,000 workers, and in accordance with statistical rules, an enquiry should have covered a minimum of 30 firms in each country, or a total of 200 firms. In fact, Prof. Melman only visited 15 large firms, and gave no indication of how these firms were spread over countries or branches of the industry. Other information upon which the report was based was supplied by about 100 experts including buyers, technicians, directors, and editors. The report, moreover, is not systematic, contains contradiction, and is of quite unnecessary length. The recommendations for the West are briefly as follows:

(a) Application of mass-production methods.(b) Elimination of technical backwardness.(c) Standardization and unit construction.

(d) Development of numerical control.
(e) Reduction in limits of accuracy and quality.

(f) Reduction in power.

(g) Reduction in number of types to increase

productivity.

In connection with (a), it is unfortunate that no figures were given to indicate what is to be understood by mass production, and that there was no suggestion as to where the resulting quantities would be sold. To justify the criticism, however, constant reference is made to Soviet industry, although, as far as is known, the only example of mass production in the U.S.S.R. is provided by the lathe plant in Moscow, which is probably producing (today) 12,000 lathes annually, of a single type. The adoption of the Melman recommenda-

tions in this respect presents no technical difficulties, but there remains the question of marketing. In the machine tool industry, there is no need for mass production such as is required, for instance, in the motor car industry. Prof. Melman has succumbed to the idea that the economic law relating to consumer goods—that a lower price creates a bigger demand—will apply in this connection. Even the drastically reduced prices at which machines from the communist bloc have been exported to the West, however, have been insufficient to create any mass market for them.

Machine tools are not products which can be sold by mere catalogue description without special equipment. Any machine tool specialist knows that the more extensive the special equipment ordered in connection with any machine tool, the more likely it is that the machine is required by a works engaged in mass production. Whether the basic machine is produced in small or large batches, assembly and the provision of equipment for given duties will alway require special attention. Moreover, the demand for such specialized machines will inevitably become greater in the future however happy machine tool builders would be (if they had a choice) to be spared these difficult and costly orders, and permitted to concentrate upon series production, which is easy to supervise and lends itself to long-term planning. A table is included (not reproduced here) to show that in West European countries with the highest outputs of machine tools, total quantities of given machines are only modest, and would not permit series production on the scale of 10,000 per annum, even in connection with the types most commonly used.

Prof. Melman complained that the industry was backward, and that insufficient support was given to research. Dr. Eisele comments: Is it believable that machine tool specialists are so backward in their own domain when for more than 60 years they have proved themselves capable of solving the production problems of their customers such

as the motor vehicle industry?

European industry is reproached for having taken advantage only to a limited extent of standardization and unit construction, but here again, Prof. Melman has omitted to submit concrete examples. It is true that there are factories where standardization of parts could be extended, but very often the rate of development of types does not justify too great an expenditure of technical effort in this direction. Nevertheless, the majority of medium and large undertakings have, for decades past, developed and used their own standards, alongside the D.I.N. standards, to the limit of what is economically possible. In the same way, unit construction has been employed for decades for such elements as gearboxes, drives, clutches, hydraulic units, and switchgear.

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The development of numerical control is constantly presented as if its introduction would result in a considerable increase in productivity, and it is complained that only a few firms have been active in this connection. The truth is that a steadily increasing number of firms has been so occupied for years, as could be seen at the 5th European Machine Tool Exhibition in Hanover in 1957, and the 6th in Paris in 1959. This fact has not been appreciated as Prof. Melman has only visited a few works. Further extension of numerical control in the field of machine tool building will only have limited possibilities in the near future, otherwise it is certain that it would be largely used in the machine tool industry of the United States, which is not the case, any more than it is in the U.S.S.R.

In certain paragraphs of the report, where Prof. Melman criticised unduly close limits and high quality, he touched on matters to which the industry is specially sensitive. It is precisely to this constant striving for increased accuracy and high quality that a great part of technical progress in general is to be attributed. While it is usually an absorbing and costly undertaking to develop and maintain a given standard of accuracy in a works, once this standard has been attained, there would, generally speaking, be no particular economy to be achieved by reducing standards to a lower level, and without such economic reasons it would be unreasonable to expect a firm to renounce such an important aspect of the superiority of its products. Experience of "war-time finish" was not, on the whole, encouraging.

The excessive power provided on Western machine tools, which Prof. Melman criticized, has often been discussed in various quarters during the last few decades. It is well known that, under actual working conditions, machines, in general, operate well below the limits of the power available because the majority of pieces to be machined do not demand that power, although the dimensions of such pieces may necessitate the use of a machine of a certain size. The maker is therefore always confronted with a choice. He may either equip a

machine of a certain size with a motor of a power which is only sufficient for the average run of work, or may provide for the maximum. The decision reached is generally in favour of the latter, by the correct process of reasoning that the price of a machine depends essentially upon its size and equipment, and that the resulting economy from installing a smaller motor would only be insignificant, whereas the potentialities of the machine would be considerably curtailed. Consequently, the majority of makers as well as buyers prefer a drive that will meet maximum power demand.

Of all the recommendations and criticisms contained in the Melman report, only these concerned with rationalization of types and manufacturing programmes can be taken seriously as being partly capable of realization. These recommendations relate to: a reduction in the variety of machines covered by the production programmes of individual factories; a reduction by amalgamation of the number of works; development of unit construction; and concentration of production in specialized works (which would be difficult to arrange). Except in a state of emergency, there is no possibility of achieving these results in a democracy by Government decree, but only by voluntary agreement, encouraged possibly by example and by fiscal means, as far as anti-trust legislation will permit. Similar recommendations have been made in various quarters in the past, and they have been successfully carried out by such groups as V.D.F. and W.E.B.O. There have been, moreover, two tendencies of late which justify a certain optimism in this respect, namely: (1) the standardization of constructional units which was brought about with unexpected speed in 1959 as a result of pressure exerted by buyers in the motor vehicle field and under the aegis of V.D.I. (Association of German Engineers); and (2) the politico-economic competition of the Eastern bloc which is becoming more pronounced and is not to be countered by traditional methods. It would be a matter for congratulation if, amongst all the unjustified attacks and reproaches of the Melman report, these recommendations, which are at least partially capable of achievement, could help to accelerate a rationalization of manufacturing programmes which should not be too long deferred.

THE U.S.S.R.

Prof Melman makes reference to the Soviet machine tool industry very frequently, and although he states that at one end of the scale there are works producing in small batches by methods which are far more unproductive than any in Western Europe, his main emphasis is on factories producing on mass-production lines. In this respect, he has probably been the victim of propaganda, since, as has been previously mentioned, it appears that there is only a single works of this type. This example, moreover, could not, in any case, be duplicated in the West, where the total production is not notably higher than the output of

this one factory.

As regards research, E.N.I.M.S. and Tsnitmasch certainly have large staffs, well equipped buildings, and massive annual budgets, and have done valuable work. It would, however, be wrong to regard these institutes as being engaged merely in research work, as they are largely occupied with design and constructional projects, which, in the West, would be carried out in the machine tool factories. The design departments of Soviet works are generally very small, and do not reach the Western average. It may be noted, for instance, that the automatic production line for gears in the Moscow lathe plant was designed and built by E.N.I.M.S., whereas in the West, no one would think of allocating such

work to a research institute. It is impossible, in the course of a short visit, to estimate the proportional division of an institute's activities between real research and other objects.

It must be recognized that the Soviet machine tool industry is concerned with a much smaller number of types than are the industries of the West, but this position is not attributable to any sudden programme standardization. It is, in fact, a planned feature in an industry which is state-controlled and which, for a long time past, has operated under its own Minister.

CONCLUSIONS

At the end of the German examination of the report, regret is again expressed that the enquiry was not undertaken by a machine tool specialist, and that, in consequence, it contains so many judgments and controversial propositions that there is little or no chance of utilizing it in the European industries, apart from certain points.

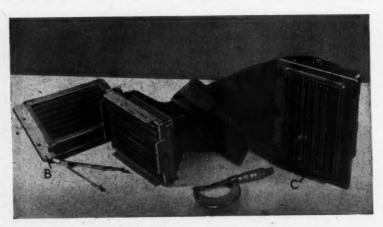
Contour Cable

The Hughes Aircraft Co., U.S.A., have developed a new type of flat and flexible conductor known as "contour cable", which weighs little more than half as much as conventional wiring. It is a ribbon-like, multi-channel, cable, formed by embedding thin, flat, metallic strips in a plastics dielectric, and up to 40 separate conductors can be incorporated.

This cable, originally introduced to save weight and space in missiles, is shown in the accompanying illustration applied to a plug-in test unit. The assembly incorporates 16 cables, grouped in eight pairs, with 36 conductors in each, making a total of 576 separate connections. The pairs of conductors are attached to contacts in insert cards in the unit A, and they plug into the connector seen on the left at B. The contact unit at the opposite end of the cables is shown plugged into its connector, at C. The length of the cables connecting the contact units is 26 in., and in this distance, the cables are bent through 90 deg., and twisted 270 deg., when in service.

As an indication of the possible savings in weight, it may be noted that 1,000 ft. of conventional 20-conductor, 22-gauge, aircraft cable weighs 82 lb., whereas the same length of contour cable having the same current carrying capacity, weighs 52 lb.

Another advantage that is claimed for the contour cable is that it can be provided with an adhesive strip on one side, as a means of attachment to the wall of a missile, or to the fuselage or wing of an aircraft.



Contour cable developed by the Hughes Aircraft Co.

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WADKIN, LTD., Green Lane Works, are experiencing a steadily rising demand for their extensive range of woodworking machinery from customers in this country and in various overseas markets. Many orders are also being received for highspeed routing machines for non-ferrous metals and we may note that one of the smaller machines in the range—the LC 6—is in regular production. Interest in tape-controlled drilling machines is increasing and several are under construction or in course of development. These machines are offered with Airmec Autoset co-ordinate setting equipment, or, alternatively, with E.M.I. electronic positioning equipment. Large automatic machines for producing parts for the furniture industry and other branches of the woodworking trade are in progress in the shops.

Several new machine tools have been installed during the past year, including a Cincinnati No. 3 dial-type milling machine and Ward No. 7 and 3 DS capstan lathes. In addition, a Kendall & Gent plano-milling machine and a screw thread whirling machine are on order. A 2-storey works extension with 9,000 sq. ft. on the first floor and a

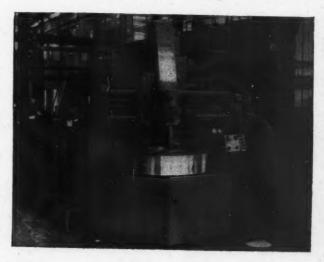
somewhat larger area on the ground floor, is shortly to be built. The Bursgreen works at Durham are also to be extended to provide additional space for the production of light woodworking machinery.

ADCOCK & SHIPLEY, LTD., Ash Street, report a heavy demand for standard horizontal and vertical milling machines, and radial drilling Bridgeport turret mills, machines. built under licence, are being supplied to many engineering firms, and it is stated that for certain applications these machines are operated at spindle speeds ranging from 650 to 10,000 r.p.m. Home sales of the company's machine tools are maintained at a high level and steady progress has been made in developing export trade with Germany. In this connection it is reported that the company is often able to reduce freight charges by care in the choice of packing, method of transportation, and routes between the works and destinations abroad. The first stage of the building expansion programme has been started, and an extension with a floor area of 25,000 sq. ft. is now under construction on an adjacent site, which is scheduled for further development as and when required.

S. Russell & Sons, Ltd., Bath Lane, report active conditions in all departments. The machine tool section is busy with orders for saw sharpening machines and Hydrofeed cold-sawing machines; also high-speed cutting-off machines provided with bar stillages and designed for production runs. The

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This Webster & Bennett type EH boring and turning mill, which is installed in the works of Villiers (Tool Developments), Ltd., Waddens Brook, Wednesfield, Staffs., has a 72 in. diameter table. It is shown set up for machining the 20½-in. bore of a 62-in. diameter gear blank of En.24 steel, which weighs 45 cwt. A good finish is obtained in the bore at a table speed of 30 r.p.m. The 11½-in. wide peripheral face of the work is machined at 15 r.p.m. with another turret tool



NF 2 cutting-off machine, for example, is suitable for repetition cutting of bars and sections of nonferrous metals or plastics. Numerous orders are received for special purpose machines and in this category we may note a robust machine for sawing

copper billets.

The foundry is well occupied with a wide variety of castings in ductile (spheroidal graphite) iron, also Ni-Resist and Ni-Hard irons. Large quantities of castings for machine tool beds and frames are also made. The structural steel department is still very busy. A new 3-storey office block, which is scheduled for completion during the autumn, is intended to serve as an administrative centre for the various departments of the firm, and will provide some 13,000 sq. ft. of floor space.

FREDERICK POLLARD & Co., Ltd., St. Saviour's Road, have a very good order book for their standard ranges of single- and multi-spindle,

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Ultrasonic examination of steel forgings by manual methods has been carried out for some time at the Atlas Works of Thos. Firth & John Brown, Ltd., Sheffield, 4. Recent trends in connection with electric power generation, however, have increased the importance of such tests. Rotor forgings are now larger and heavier, and more highly stressed, and it has become essential to ensure that no defect which could cause failure in service is allowed to pass undetected. For these large forgings manual manipulation is impractical, and the special automatic rotating equipment shown in the illustration has been installed in the heavy machine shops

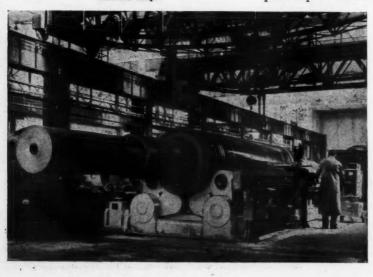
bench and column type, vertical drilling machines, heavy-duty drilling machines, and radial drilling machines. There is also a sustained demand for special drilling and boring equipment, including high production machines equipped with tooling and fixtures.

Premier Screw & Repetition Co., Ltd., Woodgate, are working to capacity on the production of precision turned and threaded parts from bar stock. Large numbers of screws made of stainless steel, free cutting mild steel, and brass, for example, are regularly produced for the instrument industry. Parts can be machined to A.I.D. and A.R.B. standards and we may note that there has been a steady growth in recent years in this class of work. Petermann Swiss-type automatic machines are widely employed.

Ex-Cell-O Corporation (England), Ltd., Hastings Road, are still busy with home and export orders for standard and special fine boring machines. Included in the current building programme is a machine for bore-grinding small ball bearing races in a 12-sec. cycle time, the parts being fed automatically to the work station. The Bryant Centalign grinding head fitted to this machine operates at a spindle speed of 44,000 r.p.m. and is arranged for automatic wheel dressing and feed-back control for size correction. An in-line transfer machine with six machining stations, and two others for flushing and gauging, is being built for turning and fine-boring centrifugally cast wet liners for internal combustion engines. planned production is 50 liners per hour.

> PERCY MARTIN, LTD., Melton Road, who deal in a wide variety of new a n d reconditioned machine tools, are still very busy as a result of the sustained heavy demand for centre lathes, drilling machines, grinding machines, and milling machines, also other types of production equipment. This company has other premises at De Montfort Street.

> WYVERN MACHINES, LTD., Percy Road, are steadily occupied with the production of 17-in. swing centre lathes, some of which are equipped with copying



attachments; capstan lathes; Wyvomatic automatic duplex turning, facing, and boring machines; and special-purpose Wyvomatic machines, including one with four facing heads, hydraulically-operated tool slides, and pneumatic work clamping. Standard Wyvomatic machines are provided with two spindles, separately driven at speeds up to 3,500 r.p.m., in either direction, by V-belts from 3-h.p. motors. Internal and external profiling facilities are afforded by template-controlled hydraulically-operated copy turning equipment. The vertical tool-slides, which are employed for undercutting, facing, or grooving, may be sequentially controlled.

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G. ELTHERINGTON & Co., LTD., Burdwell Works, Brockholes, Near Huddersfield, inform us that there has been an increasing volume of business in used machine tools in recent months and that in addition to those from the home market, a number of export orders has recently been received from various countries including India and France. Machine tools at present in stock at the works include a number of Minganti turret lathes.

H. Armitage (Machine Tools), Ltd., Town Top, Kirkheaton, Huddersfield, are maintaining a steady output of all their products. A number of export orders, for example, from New Zealand and Kenya, has recently been received for the company's 4-in. centre bench lathe, and there is a steady call for the 5-in. dividing heads.

Other activities include the production, on a contract basis, of press tools, jigs and fixtures, and special hospital equipment. Several orders are at present in hand for polishing machines for use in metallurgical laboratories.

Brook Motors, Ltd., Empress Works, Huddersfield, are busy with the production of all types of electric motors ranging from fractional horse-power sizes up to 650 h.p. Demand for domestic appliance motors has increased in recent months and the control gear manufacturing department reports that a large volume of special control panels is at present on order and in production.

The range of %- to 40-h.p., D-type, totally enclosed, fan cooled, squirrel cage motors is in good request, and recent developments in this connection have included the introduction of machines of higher horse power.

This company has produced a booklet covering the industrial range of motors, which provides useful information on the various types of units and their applications.



This Fort-Wayne automatic stator winding machine has recently been installed in the Barnsley factory of Brook Motors, Ltd.

A Fort-Wayne automatic stator winding machine, which has been installed in the Barnsley factory, is shown in the illustration.

J. Parkinson & Sons (Shipley), Ltd., Canal Ironworks, Shipley, report an increasing call for their range of machine tools and equipment from customers in both the home and export markets. A large volume of orders is at present in hand for all the milling machines in the company's range and particularly for the vertical types. Orders for Sunderland gear planers are also satisfactory, and a considerable percentage relates to machines of the larger sizes.

Demand for cutters for use with the Sunderland gear planers is continually increasing, and we are informed that business in vices is also expanding at a satisfactory rate.

The company has recently installed a number of new machine tools, including a Churchill internal grinder, and a Wadkin, articulated arm, high speed milling machine, also a Delapena induction hardening machine.

JOHN ROBSON (SHIPLEY), LTD., Ives Street, Shipley, inform us that their range of horizontal diesel engines, in sizes from 11 to 150 h.p., is still in good demand, orders at present in hand being almost entirely for export to various countries,

including Iran, Syria, Jordan, Burma, and Pakistan.

We understand that a prototype 4-cylinder, 100 h.p., vertical type diesel engine is at present undergoing tests. A Kitchen-Walker E.2. 4-ft. radial drilling machine has recently been installed in the works.

W. B. & U. ATKINSON, LTD., Rosse Street Works, Shipley, are busy with the production of all types of textile machinery components, including tensioning units and thread guides. A large order has recently been received for equipment for export to the U.S.S.R., also an order from New Zealand. To meet the increasing demand for these products, the company has installed a number of special purpose machines in recent months.

FRANK WIGGLESWORTH & Co., LTD., Saltaire, Shipley, inform us that the call for their many products is maintained at a high level. A good volume of orders is at present in hand for the company's power transmission equipment, which includes Texrope V-belts and pulleys, mechanically operated clutches of both ring and multidisc high speed types, centrifugal clutches, and flexible couplings. The foundry is well occupied with the production of the various castings required for these products.

R. SUTCLIFFE.

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VISUAL PLANNING SYSTEMS, LTD., Athlon Road, Alperton, Middlesex, have specialized since 1945 in the construction of scale models for factory and plant planning, whereby a sense of realism is conveyed by the 3-dimensional presentation of proposed machine tool layouts, production lines, and processing equipment, for example. Many large firms, and various Government Departments and educational authorities, have been supplied with simple or elaborate models in which details of door and window openings, partitioning benches, conveyors and machine tools have been reproduced to a scale of either 14 in. or 18 in. to 1 ft.

The wide range of models available from stock or at short notice covers most of the machine tools built during recent years by British, American and European manufacturers. Special models, for example of transfer machines, can be provided if required, and we may note that such an item was included in a layout depicting the proposed arrangement of some 800 machine tools in a new factory which is to be employed for the production of automobile transmission equipment. Larger

models of machine tools, to a scale of 1% in. to 1 ft., are made for display at exhibitions and for other sales promotion purposes.

Another activity of this company is the pro-

duction of castings to close tolerances in LM 6, LM 8, LM 11, LM 15, WP and DTD 5008 light alloys. A speciality is the casting of thin blading and shrouded impellers, also waveguides in LM 4 alloy by a special process which, it is stated, enables dimensional limits of ± 0.002 in. to be maintained.

A wide variety of machine tools (such as Wadkin and Bridgeport vertical millers) which are specially suitable for the accurate machining of nonferrous components is employed in the works and Hauser jig boring machines are installed under controlled conditions.

A growing demand is reported for the reclamation service provided for the removal of broken taps and twist drills from machined parts with a

Marbaix M 58C disintegrator.

Woking, Surrey LTD., Chobham, Метсо, (formerly Metallizing Equipment Co., Ltd.), are experiencing a good demand for flame spraying equipment and associated materials to be employed in connection with their three methods of applying metal or ceramic coatings to a wide variety of

The original process for the spraying of metals from a gun fed with wire is widely employed, but two additional methods of deposition, known by the registered trade marks Thermo-Spray and the METCO Plasma Flame Spray, are now being applied on an increasing scale. With the former method, coatings are built up from nonoxidizing materials in a powdered state, oxy-acetylene or other gas mixtures being employed as melting and propelling agents, whereas with the latter an electric arc shrouded by an inert gas provides zones with temperatures stated to be as high as 16,650 deg. C., to vaporize powdered materials such as aluminium oxide, cobalt, tungsten, and titanium oxide.

The range of materials that can be sprayed is steadily being extended, and we may note, for example, that cermet coatings are being applied to components that are subjected to blast erosion and chemical corrosion. Applications of flame spraying that are now well established include the coating of rocket nozzles and nose cones; vacuum tubes; high melting range crucibles; plug gauges; turbine shafts; crankshaft; and steel structures. To afford a complete service to users and potentional users of flame spray equipment, increased demonstration, training, warehouse and office facilities have recently been provided, and the next stage of the factory expansion is well under way.

BARRON & CROWTHER, LTD., Eastleigh, Hants., are extending their works and are to install additional equipment to provide improved facilities for building the well-known Barcro range of wire drawing machines. Barcro type BB machines, introduced ten years ago, are widely employed in this country and other parts of the world for drawing wires of ferrous and non-ferrous metals, including stainless steels, nickel chromium steels, carbon steels, Monel metal, aluminium and its alloys, copper, and brass. More than 1,000 of these machines are reported to be in operation, and numerous orders are in hand. Installations have been provided for producing wire in coils or spools at finishing speeds, for small diameters, of 3,000 to 3,500 ft. per min.

Barcro machines provided with 2-tiered BB drawing blocks, which prevent axial twisting of the wire and enable finished coils to be removed while wire is accumulating, are built in four sizes and each may be equipped with any number of blocks, as required. In the accompanying illustration is shown an 8-die composite machine which accepts 5 s.w.g. or 8 s.w.g. steel wire and reduces it to minimum diameters of 0-072 in. and 0-053 in. respectively. Seven 30-h.p. fixed-speed motors and one 35-h.p. variable-speed motor are employed for driving the drawing blocks of this machine.

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Composite wire drawing machine designed and built by Barron & Crowther, Ltd., Eastleigh, Hants.

Activities of Burnley Aircraft Products

Burnley Aircraft Products, Ltd., Fulledge Works, Burnley, Lancashire, inform us that the section of their works concerned with the production of aircraft components and gas turbine combustion equipment is at present extremely busy. The many activities include the fabrication of stainless steel and Nimonic components for gas turbine exhaust units and piping, and the fabrication of components from heat resistant metals, for use in nuclear power plants.

In the metal spraying department equipment is installed for the application of aluminium, copper, zinc, cadmium, nickel, molybdenum, and steel, also a number of shot blasting machines of various capacities. Other equipment provided includes a number of spark erosion machines which are employed for various duties. At one set-up on such a machine, 12 slots 0.025-in. wide, and 12 holes of 1/2 in. diameter, are produced in a Nimonic 80 component approximately ½ in. thick, the operation being completed in 35 min.

Among machine tools and equipment recently added to the plant may be mentioned a Denham S.R.10.V. centre lathe designed for machining Nimonic; a Churchill cylindrical grinder; and an automatic seam welder for producing large diameter cylinders. This latter machine was built

in the company's works and the automatic control gear was supplied by F. Hirchmann, London.

Universal Boilers, a subsidiary of Burnley Aircraft Products, make all types of road tankers. They also undertake maintenance of tankers, and offer a heavy fabricating service, on a contract basis, to the engineering industry. To meet increasing demands for this service the department will shortly be moved to larger factory premises at Ormskirk, Lancashire.

Another subsidiary, Solar Weld Languepin, Ltd., produces and markets B.A.P. Pneustroke resistance welding machines and equipment. Standard machines up to 70 kVA., and special-purpose machines up to 100 kVA rating are at present being built. In addition, the company acts as sales agent for the United Kingdom for the larger resistance welding machines made by La Soudure Electrique Languepin, of Paris.

Solar Weld Languepin also supply small special - purpose, multi - head, transfer type welding machines which are individually designed to customers' requirements. In addition, a section of the works is constantly occupied with the conversion and repair of all types and makes of special-duty welding machines.

This company recently obtained the United Kingdom sales agency for the range of spark erosion machines made by La Soudure Electrique Languepin, and in view of the great interest that has been shown by various branches of the engineering industry, production of these machines has now been started at the Burnley works.

A section of the works has been converted into a demonstration department in which spark erosion machines are shown to prospective customers, and technical assistance is given in connection with the production of particular workpieces by the spark machining process.

Large Pressurized Clean Room

What is believed to be the largest pressurized "clean section" in the country is approaching completion at the Stockport, Cheshire, premises of Fairey Engineering, Ltd., a member company of the Fairey Group. The clean section, which is in two parts, has an area of 19,000 sq. ft., and, together with the changing rooms and special canteen room, is provided with an Isora, airtight, translucent ceiling, supplied by Isora Illuminated Ceilings, Ltd., Bedford Avenue, Slough.

This ceiling comprises a light steel grid, suspended from the roof trusses of the building, and translucent panels, which are individually clipped down on to plastics sealing strips. Apart from

A view of the new "clean section" for assembly of atomic power station equipment at the works of Fairey Engineering, Ltd.

preventing the ingress of dirt, the ceiling will substantially reduce heat losses.

The clean section will be employed by Fairey Engineering for the final assembly of control rod units and burst slug detection gear for the nuclear power station which is being built at Trawsfynydd, North Wales, by Atomic Power Constructions, Ltd.

Overseas Trade in Metal Products

(Continued from page 291)

in export markets have been partially offset by falls in other directions. For example, the value of exports of "coal, coke and briquettes" dropped from £62·4 million in 1956, to £14·1 million (annual rate £28·2 million) in the first half of 1961, and the value of "cotton yarns and woven fabrics" from £88·7 million to £30·9 million (annual rate £61·8 million). Obviously, however, adverse movements on this scale cannot continue indefinitely, and it appears that if the rate of expansion of exports of metals and metal products can be sustained, a more satisfactory overall growth of export trade can be anticipated in the future.

On the other hand, if exports of metal products on the scale envisaged are to be achieved within the next decade, and the requirements of the home market simultaneously satisfied, both the capacity and the productivity of the metal working industries generally must be increased more rapidly than in the past. Clearly, a much larger output of machine tools will be necessary, and, at the

same time, further improvements in accuracy and productivity must be sought. It seems essential, therefore, that no efforts should be spared to improve facilities for machine tool research and development, both nationally and on the part of the builders of such equipment, and that the Government should adopt a more enlightened fiscal policy in order to encourage the installation of new plant, of higher potential output, on the widest possible scale.

ELECTRICITY OUTPUT CAPACITY for public supply in Great Britain had increased to 30,208 megawatts at the end of May, new plant of 320 megawatts having been brought into commission during the period. At the end of 1960, the capacity was 29,575 megawatts.

Amigo Hopper Feed Unit

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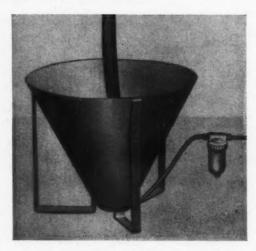
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To facilitate loading and topping-up of overhead feed hoppers, Amigo Machine Co., Ltd., Skylon House, Park Royal Road, London, N.W.10, have introduced the simple unit shown in the accompanying illustration. It is applicable to any granulated and free-flowing powder, and was originally developed by the company for use on their blow-moulding equipment.



Amigo hopper feed unit which is operated by compressed air

As may be seen, the unit comprises a container which can be placed on the floor or at any convenient point for accepting raw material from a bulk source. This container is connected by a large-bore flexible tube to the hopper on the machine to be served. Air at a pressure of about 60 lb. per sq. in. is fed into the bore of the flexible tube by way of a pipe which enters the base of the container. The air nozzle arrangement is such that the material is carried upwards in the air stream, and it is stated that lifts up to 7 ft. can be obtained, the capacity depending upon the air speed.

The Total Exports of Machinery of all types (other than electric) during the first six months of this year were valued at £419,007,990, as compared with £365,368,341 for the same period in 1960. Of this total £27,429,863 went to Australia, £26,739,388 to Canada, and £24,271,299 to the U.S.A.

Machine Tool Exports and Imports

EXPORTS OF MACHINE TOOLS

Type of Machine	Month ended May 31, 1961 Value £	Five months ended May 31	
		1960 Value	1961 Value
Bar and chucking auto- matics	91,044	313,479	507,764
Vertical	41,321	181,058	533,025
Other	90,149	689,752	451,444
Drilling machines	104,076	616,509	643,290
Gear-cutting machines	116,109	453,011	418,020
Grinding, lapping and hon-			
ing machines	234,610	1,163,526	1,470,160
Lathes: Capstan and turret	242,949	839,258	1,344,256
	351,262	1,698,111	1,870,402
Other	184,101	858,498	1,179,147
Planing machines	29,505	100,332	174,979
Presses:		10000	
Hydraulic	62,045	723,913	407,098
Other	96,202	765,896	583,756
Punching and shearing ma-	40 401	240.047	346.71
chines	48,401	249,947	340,71
Other plate and sheet- metal working machines,			
including straightening			
rolls	31,789	302,940	317,075
Screwing and threading			
machines	71,026	327,017	414,69
Shaping and Slotting ma-			104.04
chines	15,975	174,616	196,96
All other machines	262,923	1,016,427	1,515,74 366,41
Jsed, complete	75,002	1,270,697	1.831.64
arts	329,851	1,2/0,09/	1,031,07
Total	2,478,340	12,224,426	14,572,59
Destination			
Jnion of South Africa	123,140	509,490	702,88
ndia	257,272	1,475,578	2,082,03
Australia	331,801	2,758,968	2,114,21
New Zealand	54,036	187,941	359,970
Canada	124,323	580,859	678,47
Other Commonwealth coun-	121 027	690.815	831,720
tries	121,037 63,047	198,651	466,38
Sweden	98,772	259,343	513,17
Western Germany	151,631	354,796	760.78
Netherlands	50,787	224,989	375,950
France	142,242	704,327	636,69
Spain	106,156	223,658	406,58
taly	228,437	305,556	999,44
United States of America	140,162	1,175,391	556,47
Other foreign countries	485,497	2,574,064	3,087,79

IMPORTS OF MACHINE TOOLS

Name and a second			
New, complete:— Bar and chucking automatics	77,414	241.228	393,652
	160,137	634.314	653,093
Boring machines			180,204
Drilling machines	24,165	107,470	
Gear-cutting machines	128,434	311,234	1,092,144
Grinding, lapping and hon-		150	
ing machines	377,655	1,514,184	2,149,521
Lathes	233,334	803,131	1,422,189
Milling machines	313,095	1,178,600	1.324,929
Planing, shaping and slot-		.,,	
ting machines	58,409	167,555	300,234
Presses	154,015	456,820	822,161
All other machines	506,645	1,480,735	2,673,617
		450,363	387,455
Used machines, complete	91,515		1.574.208
Parts	320,480	1,249,864	1,3/4,200
Total	2,445,298	8,595,498	12,973,407
Country of Origin			
Western Germany	780,396	2.364,959	3,552,587
Switzerland			1,410,460
	287,093	1,268,226	
US America	904,822	3,311,862	5,485,019
Other countries	472,987	1,650,451	2,525,341

Books Received

B.E.A. CLASSIFIED HANDBOOK OF MEMBERS, 1961. The British Engineers' Association, 32 Victoria Street, London,

S.W.1. 608 pp. [Price 21s.]

Now in its 32nd edition, this handbook includes notes on the objects and activities of the Association and the information service which is offered; a alphabetical list of members with full names, addresses, telephone numbers, telegraphic addresses, and particulars of products; a section devoted to members' announcements; a classified list of members' products under more than 3,000 headings; and a section devoted to trade names and marks. There are indexes to the classified list of products in French, German, Spanish, and Portuguese.

DIRECTORY OF OPPORTUNITIES FOR QUALIFIED MEN, 1961 edition. By Clive Labovitch, M.A. Cornmarket Press, Ltd., Darley House, 1 Lower James Street, London, W.1. 155 pp. [Price 8s. 6d., or 5s. with paper cover.]

Opportunities and prospects offered to qualified men and women by 140 industrial and commercial organizations, and Government Departments, are here set out in detail. A classified index summarises information about the size of the organizations, whether men or women are employed, and the areas where employment is offered. Another index refers men and women with various qualifications to the particular organizations which require recruits in these categories. The directory also contains an extensive list of continuation educational courses, and an editorial section includes articles which give a broad picture of the employment situation for qualified men and women. It may be noted that amongst the industrial companies to which reference is made, the highest demand is for mechanical engineers.

NATIONAL STANDARDS LABORATORY, C.S.I.R.O., DIVISION OF METROLOGY—ANNUAL REPORT 1959-60. University Grounds, City Road, Chippendale, Sydney, N.S.W.,

Australia. 38 pp.

This report is concerned with the work of the following sections of the Laboratory: length; mass; interferometry; electronics; and applied mechanics, covering vibration, engineering design analysis, and machining research. There is a list of papers published by members of the staff in various technical journals. Reference is made to developments in air gauging which have resulted from industrial enquiries for a non-contact method for measuring the thickness of materials such as rubber and asbestos cement. In the electronics section, a fringe counting apparatus and a line setting device are being developed, also semi-automatic gauging equipment for measuring variations in the size and position of drilled holes. In the vibration section the main activity has been the theoretical study of large seismic mountings.

METAL INDUSTRY HANDBOOK AND DIRECTORY, 1961. Published for *Metal Industry* by Iliffe Books, Ltd., Dorset House, Stamford Street, London, S.E.1. 560 pp. [Price 22s. 9d., postage paid.]

Section I of this handbook is concerned with general properties of metals, and contains much useful information under such sub-headings as: particulars of the metals,

contraction of castings, specific resistance of alloys, copper and its alloys, mechanical properties of zinc die casting alloys, tempering metals, silver brazing alloys, white metal bearing alloys, British Standard Specifications, and standard classifications for non-ferrous scrap metals. The second section is devoted to general data and tables, and the third to electroplating and allied processes.

Finally, there is a directory section which incorporates a list of trade names; particulars of metal and allied trades associations and societies and of scientific and technical institutions; a classified list of products for buyers; and a list of addresses and telephone numbers of

firms whose names are included in the guide.

SPRING DESIGN. By W. R. Berry, Ph.D., M.Sc., M.I.Mech.E., F.R.I.C., F.I.M. Emmott & Co., Ltd., 31 King Street, West, Manchester. 327 pp. [Price 40s. 0d. net.]

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To design the best spring for a given duty by conventional methods is far from easy, since a number of initial assumptions must be made. Many of the design difficulties have been overcome by the author by means of nomograms, and, generally, the book describes an approach to the subject that is original and thorough.

Practically all forms of spring are considered in some detail, including coiled tension and compression, conical, volute, cantilever, laminated, disc, and ring types, also axially-loaded springs of rectangular material, bent-wire springs, shaped springs of flat material, flat spiral springs,

and gramophone springs.

lists of such electrodes.

Nests of springs, torsion bars, fatigue conditions, material for springs, design for fluctuating and cyclic loads, shot peening, and static and dynamic loading are also discussed.

The comprehensiveness of the work and the practical outlook of the author should appeal to all designers concerned with springs.

A GUIDE TO ARC WELDING ELECTRODES. The British Electrical and Allied Manufacturers' Association (Inc.), 36 Kingsway, London, W.C.2. 96 pp. [Price 5s. net.]

In connection with the issue of a revised (6th) edition of this guide, which was first published in 1944, it is pointed out that notable technical advances in engineering construction have been made possible by welding techniques, notably in the construction of nuclear power equipment, and that with greater specialization there is a growing demand for information on electrodes.

Classified lists of British electrodes are conveniently presented, together with a key to British and American electrode standards. In addition, to assist users in their choice of electrodes for particular applications, there is a brief description of the British classification of electrodes, published by the B.S.I. as B.S.1719:1951. A more complete description of the American method of classifying electrodes is also given, and equivalent American code numbers are shown in all the classified lists. In a separate section, information is given on special electrodes, for example, for welding such materials as non-ferrous metals, cast iron, and corrosion resistant steels, and there are

Trade Publications

Precision Chains, Ltd., Clayton Lane, Manchester 11. Folder Ref. 53/0 listing steel conveyor roller chains, chain wheels and attachments. Chains with pitches from 2 to 24 in. are available, and with breaking loads up to 85.000 lb.

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THE INCANDESCENT HEAT Co., LTD., Smethwick. Leaflet drawing attention to the range of foundry plant made by the company in association with The Whiting Corporation of America. Numerous installations of Whiting dust arresters on cupolas are illustrated.

WILD-BARFIELD ELECTRIC FURNACES, LTD., Otterspool Way, Watford By-Pass, Watford, Herts. Illustrated leaflet describing the 4-kW sealed quench slipper furnace, for clean hardening small components under controlled conditions. The slipper is 4-in. wide by 6-in. long, and the 12- by 26- by 20-in. deep quench tank is equipped with an agitator and a heater. The maximum operating temperature is 950 deg. C.

Branson Ultrasonic Corporation, 37 Brown House Road, Stamford, Connecticut, U.S.A. Booklet of 14 pages entitled "Chemicals for Ultrasonic Cleaning," providing much useful information on the chemicals most commonly used for the purpose, their applications, and cleaning procedures. Fourteen different types of media, including aqueous solutions and solvents, are listed. The company is represented in this country by Dawe Instruments, Ltd., 99 Uxbridge Road, London, W.5.

THE PYRENE Co., Ltd., Metal Finishing Division, Great West Road, Brentford, Middlesex. Leaflet describing the functions and methods of application of Preperite No. 1, and Preperite No. 3, for the removal of rust from ferrous, and other corrosion products from non-ferrous materials. Information is also included on Paste Preperite for local rust removal and Pyroclean No. 201 for removing scale and sludge from heating coils in Bonderizing and Parkerizing plants.

MICROMETRICAL MFG. Co., Ann Arbor, Michigan, U.S.A. (Gaston E. Marbaix, Ltd., Devonshire House, Vicarage Crescent, London, S.W.11). Informative 8-page brochure describing the Proficorder electro-mechanical instrument for measuring and recording roundness, flatness and roughness. Applications are shown of the basic units provided for measuring flat, round, and internal surfaces. Vertical magnifications up to 50,000×, and longitudinal magnifications up to 500× can be obtained.

Hadrields, Ltd., East Hecla Works, Sheffield, 9. Publication No. 463 is concerned with "fine steels" in the form of billets, bars, slabs, and forgings, for automobile and general engineering purposes. Sections are devoted, for example, to research, melting plant, rolling mills, quality control, and forged products. In addition there are tables showing the forms in which the various steels are supplied, brand numbers with equivalent En. numbers, and compositions and properties of case-hardening and structural and general engineering steels.

B. Draper & Son, Ltd., Kingston Hall Road, Kingstonupon-Thames, Surrey. Illustrated catalogue of 24 pages, concerned with Metabo electric and hand tools made in West Germany, for which the company are sole agents in this country. Tools listed include hand and electric drilling and grinding machines; bench grinders; a combined polishing head, grinder and saw bench; impact grooving and drilling machines; orbital sanders; and portable electric saws.

STUART DAVIS, LTD., Stonebridge Highway, Willenhall, Coventry. Fully illustrated and well-presented catalogue covering the range of Red Ring air equipment. The opening section is devoted to cylinders, cylinder mountings, and hydro-pneumatic variable speed units, and includes specifications and useful general information. In the section on control valves, which follows, numerous types are covered, including 5-port valves arranged for various methods of operation; pilot or master valves; 2- and 3-port pilot valves; pressure release valves; and air flow regulators. Various air-line accessories are also listed.

IMPERIAL CHEMICAL INDUSTRIES, LTD., Nobel Division, Silicones Department, Stevenston, Ayrshire. Publication giving useful application data for Silcoset silicone rubbers. Product data sheets have also been issued for two additional Silcoset rubbers which have been added to the range. Silcoset 103 is a white solvent-free paste which cures at room temperature to a resilient silicone rubber after addition of the appropriate curing agent. Silcoset 104 is thixotropic and can be effectively applied from a caulking gun. It can be readily bonded to primed metal surfaces, and is intended for sealing, patching, and caulking.

Londex, Ltd., 207 Anerley Road, London, S.E.20. Illustrated list No. 190 describing the recently-introduced Londex type TY electronic timers, which are available with five time ranges from 4 to 120, 2 to 60, 1 to 30, 0.5 to 15, and 0.25 to 7.5 sec. The principal components comprise a multi-tapped input transformer, a thyratron, a timing condenser and resistance, and two Londex relays. Wall mounting or flush mounting instruments can be supplied. The setting accuracy is ± 5 per cent of any given setting, or ± 0.06 sec., whichever is the greater. A selector gives a choice of three different contact sequences.

HACKBRIDGE & HEWITTIC ELECTRIC Co., LTD., Walton-on-Thames, Surrey. Well-illustrated 24-page catalogue, No. DB5/6, giving details of the construction of large Hackbridge power transformers with both natural and artificial cooling. Separate sections are devoted, for example, to cooling arrangements, cores, windings, tappings, tanks and fittings, temperature indication and control, and testing. Another well-produced catalogue, No. 193/2, is concerned with the applications of Hewittic silicon and germanium rectifiers for electrolytic processing, traction, and light and power supplies. Typical rectifiers are illustrated, and information is included on electrical connections, the choice of germanium or silicon, cooling arrangements, and basic layouts.

Industrial Notes

J. C. Neville, Ltd., 34 Priests Bridge, London, S.W.14, have been appointed sole agents for the United Kingdom for the Rast expander for copper tube.

CIRCUIT MOTORS, LTD., High Road, London, N.15, are the sole agents in the United Kingdom for the Cko-Motakov (Czechoslovakian) range of portable electric tools.

SHAW PROCESSES, LTD., 25 Clyde Vale, Forest Hill, London, S.E.23, announce the formation of Shaw Processes (India) Pvte., Ltd., at Faridabad, New Delhi, in conjunction with Electronics, Ltd., of the same address.

WINSTANLEY (DIE SETS), LTD., Pershore, Worcestershire, inform us that to meet growing demand they have augmented their die set manufacturing capacity, and have increased the labour force substantially.

MIDLAND SILICONES, LTD.—The address of the Birmingham sales office of this company is now Lichfield House, Smallbrook, Ringway, Birmingham, 5. Areas covered by this office comprise the Midlands, South Wales, and the South West.

An Auction Sale of Machine Tools and miscellaneous stores will be held at the W.D. Storage Depot, Rotherway, Hereford, on August 15. The auctioneers will be Russell, Baldwin & Bright (Dept. C), 20 King Street, Hereford.

THE INSTITUTE OF WORK STUDY, 3 Cork Street, London, W.1, will hold their annual conference at The College of Aeronautics, Cranfield, from September 29 to October 1. The theme will be "The Scope for Investigation into Office and Sales Procedures." Further particulars can be obtained from the above address.

VACUUM RESEARCH (CAMBRIDGE), LTD., Quayside, Bridge Street, Cambridge, inform us that they have received a repeat order for a Camvac metallizer from Metalon A.B., Kavlinge, Sweden. This compact reel-inchamber high vacuum metallizer will be used for the production of aluminium-coated capacitor tape.

THE 2ND INTERNATIONAL PIPES, PIPELINES, PUMPS AND VALVES EXHIBITION AND CONVENTION will be held at Earls Court, London, from April 9 to 13, 1962. Full particulars can be obtained from the organizers, Scientific Surveys, Ltd., Exhibition Division, 97 Old Brompton Road, S.W.7.

Conference on Creep and Fracture.—A joint international conference on creep and fracture will be held in New York from August 25-28, 1963, and in London during October, 1963. The sponsors are the American Society of Mechanical Engineers, the American Society for Testing Materials, and the Institution of Mechanical Engineers, 1 Birdcage Walk, Westminster, London, S.W.1, from whom full particulars can be obtained.

F. Pratt Engineering Corporation, Ltd., is the title under which F. Pratt & Co., Ltd., has been re-constituted as a holding company. A new wholly-owned subsidiary, F. Pratt & Co., Ltd., has been formed to carry on the

manufacture and marketing of the company's products, and the business will be continued under that name. The address, as hitherto, is Halifax, Yorks.

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KIMBERLY-CLARK, LTD., Larkfield, Maidstone, Kent, are now marketing their Kimwipe disposable wipers in roll form. Of 2-ply construction these wipers are made from soft but strong cellulose, and are intended for the heavier cleaning operations involving the removal of oils, grease, dirt, and solvents. A roll comprises 100 sheets measuring 20 by 18 in. and is perforated.

RUSSIAN TRANSLATING PROGRAMME. A folder issued by the National Lending Library for Science and Technology, Boston Spa, Yorkshire, gives titles and subscription rates for English translations of 17 Russian technical journals. A list of Russian technical books which have been translated and published is also included. Particulars of many other translations which can be purchased or obtained on loan are available from the above address.

TECHNIC DESIGN SERVICES Co., LTD., 891 Pershore Road, Selly Park, Birmingham 29, have recently acquired the Northfield Tool Co., Ltd., South Birmingham. The manufacturing facilities of the latter firm will supplement the services of the other members of the group—namely, Technic Electrics (Birmingham), Ltd., and Viewdy Investments—and will enable the group to offer a complete consulting, design, and production service in connection with machines, fixtures, and tooling equipment.

Schloemann, AG., 13 Steinstrasse, Düsseldorf, Western Germany, who for many years have built machinery and plant for the plastic shaping of ferrous and non-ferrous metals, have extended their production programme to include twin screw extruders and injection moulding machines for plastics. The latter machines, of the heavy-duty type, have been developed in conjunction with Albert Stübbe, Vlotho an der Weser, and can be supplied with shot capacities up to 13‡ lb.

C. A. PARSONS & Co., LTD., Heaton Works, Newcastle upon Tyne, have signed a licence agreement with ZALLEA BROTHERS, Delaware, U.S.A., for the manufacture and sale of thinwall-bellows expansion joints of Zallea design. The agreement provides for the marketing of the Britishmade products in the United Kingdom, the European Free Trade Area, and British Commonwealth (with the exception of Canada). These joints are used to absorb movement in a wide range of piping applications particularly in the oil and chemical industries.

THE LAPOINTE MACHINE TOOL Co., LTD., Otterspool, Watford By-Pass, Watford, Herts., have provided an additional 1,000 sq. ft. of shop area, which has enabled the broach regrinding facilities to be enlarged and improved. As a result it has been possible to reduce the average regrinding time from three weeks to less than a fortnight. It is stated that by efficient planning it is hoped to reduce the time still more. This development forms part of a general expansion programme which is scheduled for completion in September.

LANCING MACHINE TOOLS, LTD., Commerce Way, Lancing, Sussex, have been appointed agents for the range of plate, sheet, tube, and section working machinery built by Boldrini, S.P.A., Italy. This range includes pyramid type plate bending rolls of capacities up to 20 ft. 2 in. by 1½ in.; initial pinch type bending rolls up to 14 ft. 2 in. by 2½ in.; shipyard rolls up to 40 ft. by 2½ in.; straightening rolls; tube and section bending rolls; friction screw presses for dishing ends up to 19 ft. diameter by 2 in. thick; and rotary cold flanging machines.

David Brown Industries, Ltd., inform us that a turbine reduction helical gear unit which was supplied in 1929 to the D.P. Battery Co., Ltd., Bakewell, by Park Works, Huddersfield, has been withdrawn from service because the generating plant is no longer to be operated. During a period of more than 30 years the gear unit has required no attention although the plant has been run continuously with only short breaks for routine inspection at holiday times. The unit has been employed to transmit drive from a 225 kW. turbine with a reduction from 7,000 to 1,000 r.p.m. at 12-in. centres.

THE CAMP BIRD GROUP of companies announce that production of cold forging plant has been started in a new £500,000 factory by Saarländische Werkzeug und Maschinenfabrik, Walther Nothelfer G.m.b.H., at Lockweiler, between Saarbrücken and Trier, Western Germany. In addition to the construction of cold forging equipment for sale, a complete cold forging installation will be kept in production to enable customers' plant to be proved under operating conditions. The operating company is a member of the International Cold Forging Group and is thus associated with Cold Forging, Ltd., 29 Hanworth Road, Sunbury-on-Thames, Middlesex.

CLYDE WILLIAMS CORPORATION has been formed by Dr. Clyde Williams and his American and European business associates. The headquarters are at 50 West Gay Street, Columbus, 15, Ohio, U.S.A., and there will be branch offices in London and Paris. One of the main purposes of the company will be to provide liaison between European and American technology. In this connection it is pointed out that although great progress is being made on both sides of the Atlantic, arrangements for communication and integration of technological developments have sometimes been inadequate in the past. For this reason it is planned to hasten the process of information dissemination "as it relates to research and technology, to markets for products, and to finance and investments."

MATERIALS HANDLING EQUIPMENT (GREAT BRITAIN), LTD., 40a Dover Street, London, W.1, inform us that the parent company Hunslet (Holdings), Ltd., is to allocate greater facilities to meet the growing home and export demand for their products which include Kestrel and Falcon side-operating fork-lift carriers, and Lizard electric reach trucks, and to provide for further development of existing and additional models. From August 14, production and key employees will be transferred from Maidenhead to the much larger works of the Hunslet Engine Co., at Jack Lane, Leeds. The London and Maidenhead offices will be merged and from August 21 will be located with those of the Hunslet Group in Locomotive House, 30-34 Buckingham Gate, S.W.1.

MACHINERY'S ENQUIRY BUREAU

For many years MACHINERY has provided an enquiry service not only for subscribers and advertisers but for all engineers in need of such information as the names of makers—or their agents—of machines or equipment for performing particular operations, suppliers of various classes of material, firms with facilities for undertaking certain types of work, owners of trade names, and agents for foreign machine builders. If you have such a problem write (MACHINERY, Enquiry Bureau, Clifton House, 83-117 Euston Road, London, N.W.1) or telephone (Euston 8441, 2 lines). This service is, of course, entirely free.

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MANUSCRIPTS FOR BOOKS covering all branches of engineering production will receive careful consideration and should be sent to the Manager, Book Dept., MACHINERY, National House, 21 West Street, Brighton, 1.

CONDITIONS OF SALE AND SUPPLY.—MACHINERY is sold subject to the following conditions:

That it shall not, without the written consent of the publishers first given, be lent, resold, hired out or otherwise disposed of by way of trade except at the full retail price of ls. 3d. and, that it shall not be lent, resold, hired out or otherwise disposed of in a mutilated condition or in an unauthorised cover by way of trade; or affixed to or as part of any publication or advertising literary or pictorial matter whatsoever.

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William Whiteley & Sons

Alfred Herbert, Ltd., Coventry, have acquired the whole of the issued share capital of William Whiteley & Sons, Ltd., Huddersfield. The former company has acted as selling agent for Planers planing machines for some years with the result that there has been an increasingly close association between the organizations. It was therefore decided that it would be in the interests of both if production and selling were integrated. Mr. J. Charlesworth will still hold the positions of director and general manager and production in Huddersfield will be continued and expanded.

Personal

DR. W. J. Gibbs, M.I.E.E., has relinquished his appointment as manager of the engineering mathematics department, Associated Electrical Industries (Rugby), Ltd., Rugby, but remains as a group company consultant. He has been succeeded by Mr. N. Kerrush, M.A., A.M.I.E.E.

DR. SYDNEY JONES has joined R. B. Pullin & Co., Ltd., Great West Road, Brentford, Middlesex, as technical director. Until recently he was Director of Research Applications at the Central Electricity Board, where he was responsible for the development of research projects, in particular, the development of automatic process control systems.

Mr. W. N. Collins, M.I.Mech.E., who will reach retirement age early in 1962, has resigned from the position of assistant managing director of F. Perkins, Ltd., Peterborough, and from the company's board and the boards of its subsidiary companies. It is not intended that his connection with the Group should be entirely severed immediately, but his duties will be gradually lightened.

DR. B. L. GOODLET has retired from the position of managing director of Brush Electrical Engineering Co., Ltd., Loughborough, because of ill health, but will continue with the company as vice-chairman. He is succeeded by MR. James Edward Smith, M.I.Marine Eng., formerly managing director of the National Gas & Oil Engine Co., Ltd., Ashton-under-Lyne, and a director of Hawker Siddeley Industries.

Mr. R. B. Dew, assistant managing-director of Production Engineering, Ltd., has been appointed visiting professor in industrial administration at Manchester University. It is stated that this post is the first of its kind at any British university. The Department of Industrial Administration of the College of Science and Technology was established in 1918, and the first professor, Mr. R. W. REVANS, who is now being joined by Prof. Dew, was appointed in 1955.

The following new appointments have been announced:-

Mr. O. E. Trivett, A.M.I.Prod.E., A.M.I.E.E., as general manager of Gamet Products, Ltd., Colchester, a member company of the 600 Group.

Mr. F. J. Everest, M.Sc., M.I.Mech.E., as director and general manager of Stein Atkinson Vickers Hydraulics, Ltd., 197 Knightsbridge, London, S.W.7. Mr. C. J. Powers as assistant manager of the contracts division of the industrial department of York Shipley, Ltd., North Circular Road, London, N.W.2.

Mr. F. J. SULLIVAN, as a director of Turbine Gears, Ltd., Cheadle Heath, Stockport. He was previously commercial manager of the company.

Mr. D. J. Barrow, formerly contracts supervisor for Tank Linings, Ltd., Droitwich, as production engineer of Winstanley (Die Sets), Ltd., Pershore, Worcestershire.

MR. H. Andrews, as secretary and MR. H. L. Hudson as chief accountant of Wickman, Ltd., Banner Lane, Coventry, following the appointment of Mr. H. B. Morris to the board of directors.

MR. Bernard Feltbower as chief engineer of the Control Gear Division of the English Electric Co., Ltd., at Kidsgrove, Stoke-on-Trent. He joined the company at the beginning of July.

Mr. IAN D. McDonald, technical representative of Angus & Crichton (Sales) Ltd., 7 Midland Street, Glasgow, C.1, as a director of the company, the sole representatives in Scotland for Elgar Machine Tool Co., Ltd., Press & Shear Machinery Co., Ltd., and Gate Machinery Co., Ltd.

Rockwell Board Appointments

Mr. J. M. Brice, M.I.Prod.E., Mr. H. A. Chambers, M.I.Prod.E., and Mr. H. Rockwell, B.Sc., A.M.I.Mech.E., have been appointed directors of Rockwell Machine Tool Co., Ltd., Welsh Harp, Edgware Road, N.W.2.

Scrap Metals

MIDLANDS.—When the local factories closed for holidays on July 29, trading was practically suspended for the next two to three weeks as practically all consuming works were affected.

The few exceptions include customers for cast iron scrap and bushy turnings. In particular, cylinder cast iron scrap can be delivered to foundries which are accepting material over the holiday period, to obtain increased supplies.

Prices for chipped steel turnings have fallen by a further 10s. per ton for deliveries can be resumed on a reasonable scale before August 21.

The situation as regards cast iron borings appears to be firm, and odd loads are being moved during the holiday period to chemical works in other areas.

During the interval, merchants will be carrying out plant repairs and making space in their yards to accept deliveries after the holidays, and it is expected that several grades of bundles and other scrap will have to be stocked pending the re-opening of markets.

In general, it is a difficult time for merchants, who are committed to accept scrap that is arising, at contract prices, while consumers are out of the market for periods varying from 2-4 weeks. It is not easy to be optimistic as regards demand for scrap over the next few weeks and prices offered by merchants for the occasional amounts of "difficult" grades will therefore be lower than usual.

New Companies Registered*

TURNER & STOTT, LTD., 23 Park Street, Manchester, 3. Registered July 14, 1961. To carry on the business of diamond die makers, tool die makers, jig and machine tool manufacturers, etc. Nom. cap.: £2,000 in £1 shares. Directors: Wm. F. Turner and J. Stott.

W. W. Lawson & Co., Ltd., 11 Aigburth Vale, Liverpool, 17. Registered July 13, 1961. To carry on the business of toolmakers and engineers, etc. Nom. cap.: \$\frac{4}{4},000 \text{ in } \pm\$1 shares. Directors: Wm. W. Lawson and A. W. Moran.

Graham Spark Erosion, Ltd., Library Chambers, Church Street, Lye, Stourbridge. Registered July 18, 1961. To carry on the business of tool and die makers, etc. Nom. cap.: £100 in £1 shares. Directors: Harold K. Graham and George W. Knott.

IMPACT TOOLS (HERTFORD), LTD., 110 London Road, St. Albans. Registered July 25, 1961. To carry on the business of precision engineers, etc. Nom. cap.: £4,000. Directors: C. H. Moody and M. Moody.

From the lists compiled by Jordan & Sons, Ltd., Company Registration Agents, 116-118 Chancery Lane, London, W.C.2.

Machine Tool Share Market

Quiet and mainly dull conditions prevailed in stock markets during the period under review, and the tendency was easier in nearly all sections.

The gilt-edged market remained depressed and on balance losses predominated among British Funds and similar fixed interest stocks.

Commercial and industrial markets were unsettled, and for the most part share prices moved to lower levels. Some rallying resulted from selective buying, but the general trend was adverse. Among machine tool issues Birmingham Small Arms lost 2s. at 21s. 6d.; British Oxygen, 6d. at 20s. 6d.; Coventry Gauge & Tool, 1s. 4\frac{1}{2}d. at 20s. 1\frac{1}{2}d.; Craven Bros. (Manchester), 7\frac{1}{2}d. at 8s. 3d.; Alfred Herbert, 2s. 9d. to 63s. 6d.; Kerry's (Gt. Britain), 6d. at 9s.; Newall Engineering, 6d. at 7s. 6d.; Samuel Osborn, 1s. at 47s. 3d.; and John Shaw & Sons (Wolverhampton), 1s. 9d. at 15s. On the other hand, Asquith Machine Tool advanced 3d. to 9s. 6d.; Chas. Churchill, 1\frac{1}{2}d. to 9s.; A. A. Jones & Shipman, 1s. 3d. to 23s. 9d.; and Ambrose Shardlow, 6d. to 58s.

COMPANY		Denom.	Middle Price	COMPANY		Denom.	Middle Price
Abwood Machine Tools, Ltd	Ord	1/-	1/9	Herbert (Alfred), Ltd	Ord	61	63 /6
Allen (Edgar) & Co., Ltd	Ord	(3	37 /-	Holroyd (John) & Co., Ltd	"A" Ord	5/-	20 /-
	5% Prf		13/-+		"B" Ord	5/-	18/6
Arnott & Harrison, Ltd	Ord	4/-	8/9	99 99	B Org		
				Jones (A. A.) & Shipman, Ltd	Ord	5/-	23/9
Asquith Machine Tool Corp., Ltd	Ord	5/-	9/6		7% Cum. Prf. 51% Red.	5/-	4/9
	6% Cum. Prf.	El	16/6	Kearney & Trecker-C.V.A., Ltd	51% Red.	(1)	11/-
Birmingham Small Arms Co., Ltd	Ord	10/-	21/6		Cum. Prf.		,
	• • • • • • • • • • • • • • • • • • • •	,			Prefd. Ord	£I	13/9
** ** ** **	50/ Cum	£I	14/6	Kearns (H. W.) & Co., Ltd	Ord	5/-	22/-
90 99 99 111	5% Cum.	2.1		Kerry's (Gt. Britain), Ltd	Ord.		9/-
	40/ Cum	£I	17/-	Kerry's (Gt. Britain), Ltd	Ora	3/-	31-
00 20 00 ***	6% Cum. B" Prf.	EI	11/	M M			
				Macreadys Metal Co., Ltd	Ord	5/-	16/6
99 99 99 444		Stk.	901	Martin Bros. (Machinery), Ltd	Ord	2/-	2/6
	Deb.			Massay (B. & S.), Ltd	Ord	2/-	11/-×
British Oxygen Co., Ltd	Ord	5/-	20/6			1	
			1	Newall Engineering Co., Ltd	Ord	2/-	7/6
	6% Cum. Prf.	EI.	19/-	Newman Industries, Ltd	Ord	21-	71-
Brooke Tool Manufacturing Co., Ltd.	Ord		8/104	***************************************	6% Prf. Ord.	2/-	5/-
Broom & Wade, Ltd	Ord	5/-	22/6	Noble & Lund, Ltd	Ord.	2/-	61-
	40/ C D-f	£	17/-	Nome & Lund, Ltd	Ord	2/-	86
Brown (David) Corporation, Ltd	5% Cum. Fri.	61	15/-	Norton, W. E. (Holdings), Ltd	Ord		
Brown (David) Corporation, Ltd	54% Cum. Prf.		13/-	Osborn (Samuel) & Co., Ltd	Ord	5/-	47/3
Buck & Hickman, Ltd	6% Cum. Prf.	13	17/-		51% Cum. Prf.	£1	22/-
Butler Machine Tool Co., Ltd	Ord		16/3	Pratt (F.) & Co., Ltd	Ord		18/3
99 99 99	5% Cum. Prf.	£i	12/6	Sanderson Kayser, Ltd	Ord	10/-	32/6
Churchill (Charles) & Co., Ltd	Ord	2/-	9/-		64% Cum. Prf.	£I	16/3
	6% Cum. Prf.	£	25/741	Scottish Machine Tool Corporation.	Ord	4/-	9/-
Clarkson (Engrs.), Ltd	Ord		6/-	Ltd.		1 "	1
		1	ex capt.	Shardlow (Ambrose) & Co., Ltd	Ord	13	58 /-
Cohen (George), 600 Group, Ltd	Ord	51-	11/3	Shaw (John) & Sons, Wolverhamp-	Ord	5/-	15/-
	41% Cum, Prf.	5/-	11/6	ton. Ltd.	010	3/-	19/-
Coventry Gauge & Tool Co., Ltd	Ord.	10/-	26/14xd	Sheffield Twist Drill & Steel Co.,Ltd.	0-4	41	1019
	CO/ C	13		Snemela I wist Drill & Steel Co.,Ltd.		4/-	19/3
DO DO DO	5% Cum. Red. Prf.	2.1	16/3		5% Cum. Prf.	(1)	13/3
	Red. Pri.		1 1	Stedall & Co., Ltd"	Ord	5/-	7/3
Craven Bros. (Manchester), Ltd		5/-	8/3	Sykes (W. E.), Ltd	"B" non-	10/-	28/9
Elliott (B.) & Co., Ltd	Ord	1/-	2/6		voting Ord.		
			1	Tap & Die Corporation, Ltd	Ord	5/-	16/3
	44% Red.	13	12/-	** 12 44		Sek.	824
	Cum. Prf.	-			1961-1977	-	
		1		Wadkin, Ltd	Ord	. 10/-	26/-
Firth Brown Tools, Ltd	4% Cum. Prf.	EI	10/6	Ward (Thos. W.), Ltd	Ord	. (1	67 /6
Greenwood & Batley, Ltd	Ord		20/14			13	13/6
		10,-	701.4	99 99 *********************************	lat Pref.	E.	12/0
Harper (John) & Co., Ltd	Ord	. 5/-	7 /7 xd			13	21/6
		13	11/74	99 90 000000000000000000000000000000000	5% Cum. 2nd Pref.	E1	21/0
99 99		13	11//4	MARIN I I I I			1
	Cum. Prf.	1	1	Willson Lathes, Ltd	Ord	. 1/-	1 3/-

The Middle Prices given in the list are in several cases nominal prices only and not actual dealing prices. Every effort is made to ensure accuracy, but no liability can be accepted for any error.

* Sheffield price.

\$ Birmingham price.

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PRICES OF MATERIALS

All prices per ton except where otherwise stated.

Pig iron*			MAKERS' PRICE	ES
Foundry and Forge			Hexagon Steel Bars ¹	
No. 3, Class 2			Sizes in inches from I in. up to	
Middlesbrough (10 tons or over) £2 Birmingham (10 tons or over) £2	1 17	3	2·21 and 2·41 a/f ex works, 2 tons basis	£42 17 6†
Phos. Over 0-1 up to 0-4%			Free cutting black	£46 14 6†
Birmingham (6 ton lots) (2	3 5	0	Reeled Steel Bars ¹	
Grangemouth (6 ton lots) £2	3 10	0	Single-reeled, 14 in. upwards,	
Hæmatite			f.o.t. works (+ usual extra for sizes)	£43 9 0†
English No. 1 (10 tons or or	ver)		Free cutting	£47 7 0†
	3 19	0	Precision-ground Mild S	teel¹
Scotland (made in Scotland, zone S.	5	6	I-in. diam. ± 0-00025-in.	124- 44
Sheffield £2	5 9	0	4-ton lots, per cwt. Bright Ground Stainless	124s. 6d.
		-	Steel Barel	
Welsh 10 tons or over £23	3 19	0	EN56AM (martensitic, free cut	ring)
Steel Products*				£304 10 0
Medium plates (50 tons and over) £4	3 16	6	EN58AM (austenitic free cuttin Prices are basic, subject to e	g) £377 10 0
Mild steel plates, ordinary (50 tons and over) £40		•	High-speed Steel	
Boiler places (50 tons and over) £4.	2 17	ŏ	Black random length bar. All	prices basic.
Flat bars, 5 in. wide and under (50 tons or over)	9 1	0	per lb., subject to extras:	,,,,,,,
Round bars, under 3 in. (50 tons		-	Molybdenum " 66 "	6s. 5d.
or over) Billets, rolling quality, soft U.T.	9 1	0	Molybdenum "46"	6s. 3d.
(100 tons or over) £3	1 15	6	14 per cent tungsten 16 per cent tungsten	6s. 11d. 7s. 4d.
Phosphor Bronze			18 per cent tungsten	7s. 9d.
	4 0	0	22 per cent tungsten	9s. 2d.
ingots (200) (xiiio), o,c			5 per cent cobalt	10s. 10d.
Copper			4-75/5-25 molybdenum	
Cash (mean) £230	0 2	6	+ 6.0/6.75 tungsten + 1.75/2.05 vanadium per cent	
Cold rolled and hot rolled sheets 4 ft. by 2 ft. by 10 SWG £306 10 0-£30			(3-0-2)	6s. 7d.
£306 10 0—£30 Rods, & in, to 1 in, diam. £32	6 15		Precision-ground, High-	speed
Tubes, It in, bore by 10 SWG,		-	Free-turning B	
ton lots, per lb. 3: Wire rod, black, hot-rolled	s. 2	id.	f-in. diam. ±0-00025-in., 2 tor lots, per lb.	2. 784
(1-18 in.), English £24	5 12	6	Grey Iron Rod	2s. 74d.
			Die Cast ⁴ in random lengt	he 19 in ea
Zinc Refined, minimum 98 per cer.t			26 in. rough machined in in. sixe. Extra for definite le	above listed
purity, current month (mean) £7	7 17	6	size. Extra for definite le counts for orders over £150	ngths. Dis-
Brass			Per cv	vt. net.
	. 10	114	Mark I 260s. 3d.	Mark III
Tubes, solid drawn, basis per lb. 1: Strip 63/37, 6in. by 10 SWG coils, ton lots £256 10 0—£25		14.	‡ or ‡ in. 260s. 3d. i or i ‡ in. 208s. 4d. i ‡ to i ‡ in. 146s. 3d. i ‡ to 2 in. 112s. 7d.	338s. 3d. 267s. 3d.
ton lots £256 10 0—£25 Rods, 1-3 in. diam. (59 per cent	9 10	0	1 to 1 in. 146s. 3d.	181s. 7d. 133s. 6d.
copper) 2	s. 0	₽d.	2 to 3 in. 97s. Id.	1125. 90.
Yellow Metal				105s. 3d.
Condenser plates, per ton £18	9 0	0	Continuous Cast	
		∄d.	diam. + 0.010 to 0.020 in	n., prices as
			quoted for die cast bar4	208s. 4d.
Aluminium			centreless ground 1 or 1 in. +0.010 in. Extra	
Ingots, min. 99-5 per cent Canadian d/d £18	6 0	0	for hardenable 1\(\frac{1}{4}\) in. alloy iron ⁵ 1\(\frac{1}{4}\) in. to 2 in. Per cwt. net 2\(\frac{1}{4}\) to 3\(\frac{1}{4}\) in.	146s. 3d.
			Per cwt. net 2 to 3 in.	1. 112s. 7d. 97s. 1d.
Tinplates			Stellite ⁴	
**U.K. Home trade:			Welding Rods, plain	
Cold reduced, f.o.r. makers works (15-50 tons)	3 6	8	in. diam., per lb.	30s. Od.
Cold reduced, f.o.r. makers works (15-50 tons) U.K. Export: Hot rolled basis, f.o.r.		-	Toolbits	
works port 73s. 6d.—	76s.	Od.	4 in so v in each	22s. 3d.
Works port 73s. 6d.— Cold reduced basis, f.o.r. works port 73s. 6d.—	74-	0.4	1 Colvilles, Ltd., Glasgow, and	7 Grosvenor
works port /3s. ed.—	705.	va.	Street, London, W.I. 2 Pratt, L	evick & Co.,
Gunmetal			St. Stephens Street, Birmingham	, 6. 4 Sheep-
Ingots, B.S. 1400 L.G.2, delivered			field. 8" Florast." Harold And	Irows Sheen
*Subject to increase of 1%.	9 0	0	1 Colvilles, Ltd., Glasgow, and Street, London, W.I. 2 Pratt, L Ltd., Chester. 3 Spartan Steel & St. Stephens Street, Birmingham bridge Alloy Castings, Ltd., S field. 5" Flocast," Harold And bridge, Ltd., Halscowen. 6 De Ltd., Highlands Road, Shirley, Sc	loro Stellite,
			Ltd., Highlands Road, Shirley, Sc	niihull.
**Official maximum price, after allow adjustments for increase in price of time.	wing	for	† Plus I per cent.	

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Free Cutting Steel			
Bright cold drawn:			
(Usaspead) over I to 2 in.	€59	4	61
Lead bearing (Usaled)	£63	11	01
Precision ground, 14 in.	£84	14	61
Bright Drawn			
M.S. bars (M.M.C.) over 14 to 2 in.	€56	10	Ot
Square edge flats (Usaflat)	£73		61
M.S. angles (Usaspead)	£100	-	61
Case hardening (EN) (Usacase over 14 to 2 in.	€62		Oİ.
M.S. bars (EN3B) (Usamild)	€58	-	61
over 1 to 2 in. Carbon manganese semi-free o			oî
case hardening (EN202) (Us 202) over 11 to 2 in.	£71	1	01
35/45 ton tensile (EN6) (Usen) over I to I in.			01
0-4 carbon normalized (Usaspe "40") over 14 to 2 in.	£69	5	01
0-45 carbon normalized E (Usaspead 55)		15	01
Carbon manganese steel to Spe fication ENI6T (Usaspe 5565), per ton	ici-		
Ground Flat Stock			
 18-, 24-, and 36-in. lengths speed). List prices plus 10 pe less 5 per cent. 			
Oil Hardening Cast Ste	el		
Non-shrink (Usaspead N.S.O. ‡ in. to 2‡ in., per lb.	H.),	s. 1	Id.
Non-distorting heavy duty (Usaspead H.C.H.C.), \(\frac{1}{2} \) in. to 2\(\frac{1}{2} \) in., per lb.		41.	2d.
Silver Steel			
(0·194-in. to 11-in.) Genuine Stubs quality, per lb.	M 1	. 27	1100
)d. les s. 8d.		
Boxes of 16 assorted sizes, 15 to \$ in. diam.			6d.
Stainless Steel			-0.
KE40AM (free cutting), per lb	•	38.	84

Glacier Machined Bronze Bars Phosphor bronze (288) } Prices on

Lead bronze	,	application
High-speed Steel		
10	Brices	on application

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Usaspead	"Super"	. 1	
**	"Supreme	" }	List price
	Cobalt 10	,	

Shimst	ock		
	sorted,	per tin	3s. 6d.
Brass	99	99	7s. 3d.

⁶ Macraady's Metal Co., Ltd., Pentonville Road, N.I. Subject to confirmation by London Office. Delivered free by van in London area.

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11d.

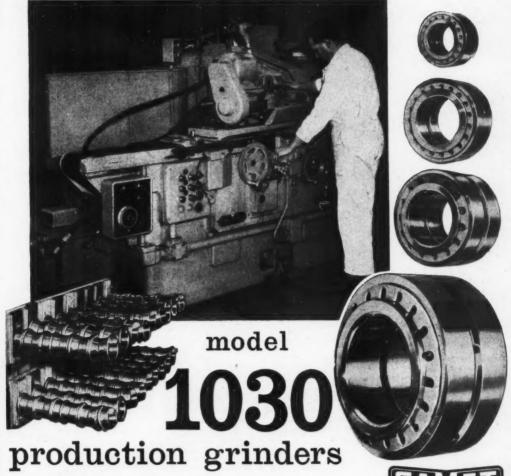
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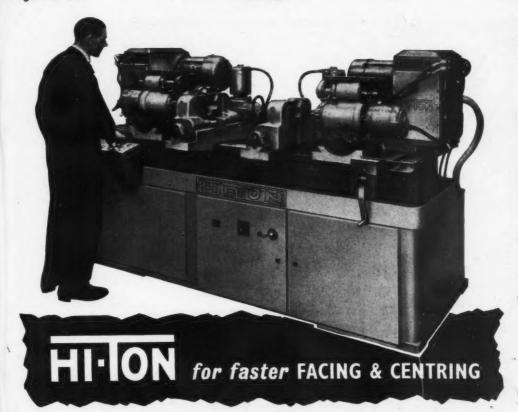
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RATION



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It is robustly constructed for heavy duty and operation is extremely simple. An automatic cycle is provided by an electrical control panel with push button for vice closing, a cycle start button causes the milling cutters to rotate, fast approach, traverse across the end faces and return. Milling cutters stop rotating and the centring spindles rotate, fast approach feed to depth and return. A push button is then depressed to open the vices at the end of the cycle.

Capacity: Max. bar length 42in. Max. overall diameter 6½in. Max. cut ¾in. each end

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Close up view of milling and centring head



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TYPE E: Knife Edge adjustable anvils for undercuts, etc. Range 0-11‡ dia.



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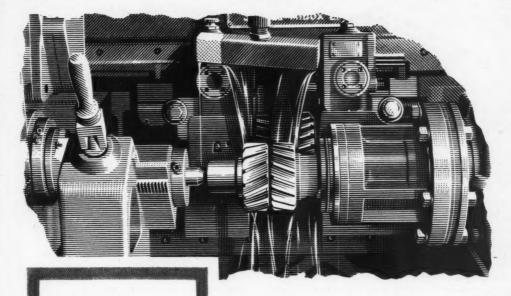
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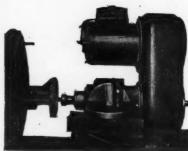


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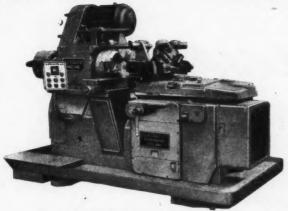
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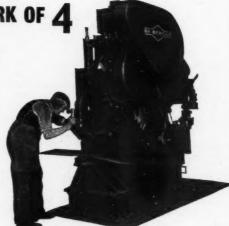
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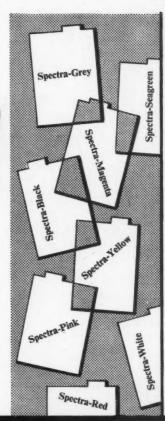
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Spectra Spectra - Color



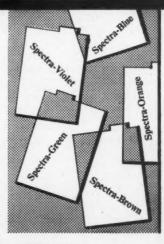
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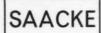


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with face grinding head

* Simple Operation

* Easy Chucking or Clamping

Specification:

Grinding capacity bores from	∔ ″—6″
Grinding length	7"
Grinding length with raised colu	ımn 11"
Dia. of work table	121"
Max. distance centre of work	table
to vertical column	113"
Internal taper of work table	M.T.
Table ewivels through	10°

Speed of work table (2)	110/220 RPM.
Grinding spindle speeds	9000/18000 RPM
Power of spindle motor	⅓ H.P.
Table motor	∄ H.P.
Hydraulic motor	∄ H.P.
Floor area of machine	32" x 30"
Height of machine	70"/78"
Nett weight	2640-lbs

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MODEL 28 AN

HEAVY DUTY GENERAL PURPOSE DRILL

With a drilling capacity of up to 2inin M.S., these machines have nine
spindle speeds up to 489 r.p.m. and
six automatic feeds, with electric
reverse if required. Ball bearing
mounted gear drive. Available in
gang drills with two to six columns
on one base. Two other models
available, with capacities of l\(\frac{1}{2}\)in.
and \(\frac{1}{2}\)in, respectively.



MODEL 21 AR

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Available in three sizes with capacities of Itin., Itin. and 2in. respectively. Similar in performance and characteristics to the box column machine.



THERE ARE 'CORONA' DRILLING MACHINES FOR EVERY DUTY FROM SUPER HIGH SPEED SENTIVE TO HEAVY DUTY SINGLE SPINDLE AND MULTI-DRILLS. CONSULT US ON YOUR OWN DRILLING PROBLEMS.



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Compact and powerful, this all-purpose mill will perform a wide variety of work from the cold rolling of a wide range of metals from lead and gold to steel and radioactive material.

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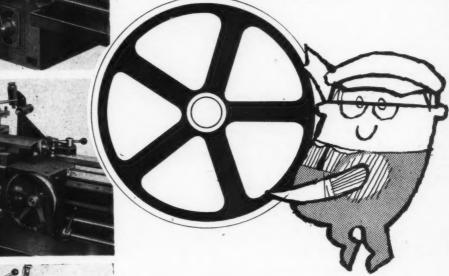
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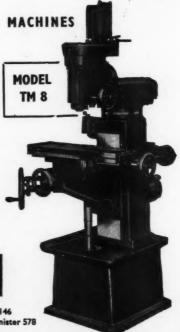
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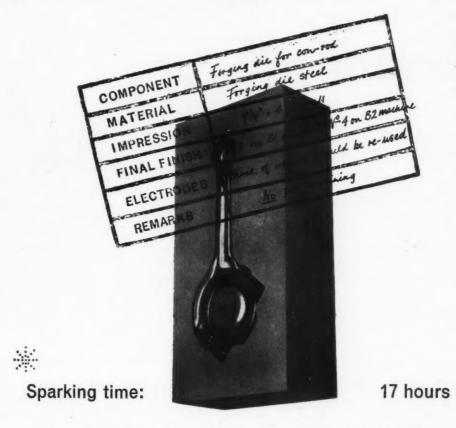
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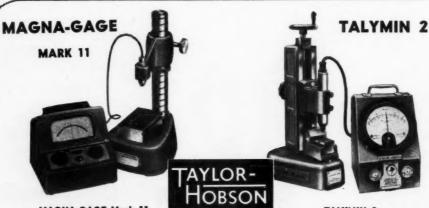
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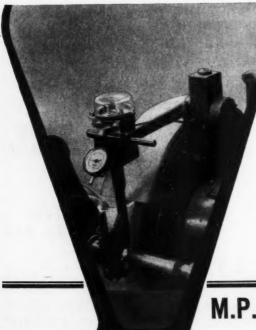
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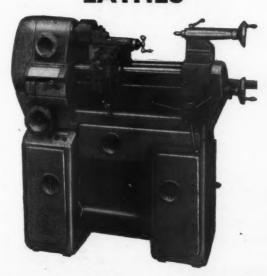




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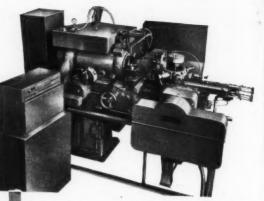


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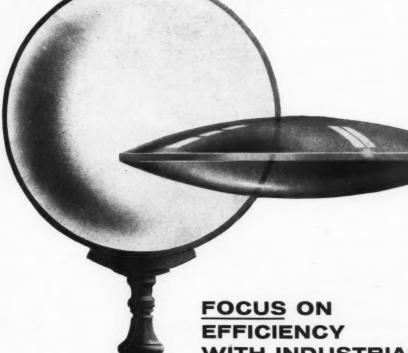
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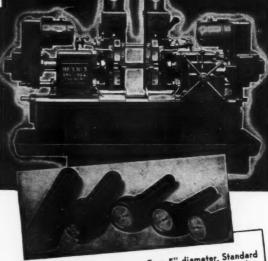
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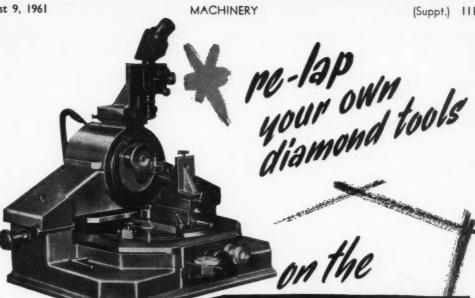
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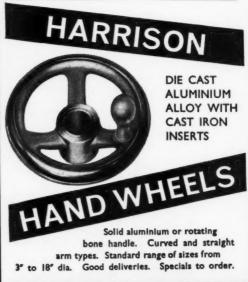
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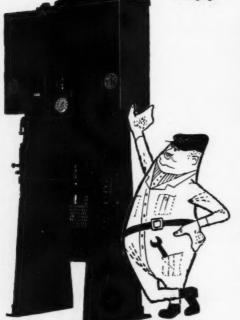
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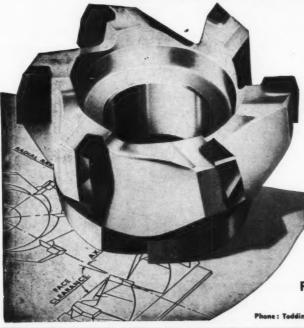
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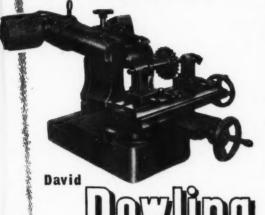
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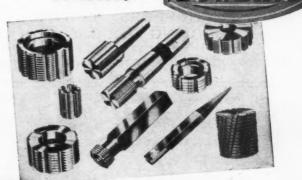
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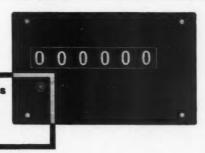
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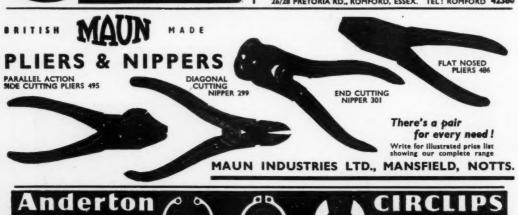
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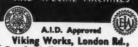
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VICTORIA No. V2 Vertical Milling Machine.
Table size 45in. × 11 in. 400-440/3/50.
Instant delivery.

CENTAUR TOOL WORKS, EYRE STREET, SPRING HILL, BIRMINGHAM, 18

Tel. EDGbaston 1118 & 1119. Capstan, Birmingham

Cam or Profile Copy Milling Machines for diameters up to 20in. or areas up to 18in. × 22in. Also Rotary End Profile Miller. All 400/3/50.—HICKS MACHINERY, LTD., 26, Addison Place, London, W.11. Tell.: PARK 2333.

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For blue and dye line prints. With
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HAVE AVAILABLE FOR EARLY DELIVERY

One NEWALL No. 0 Jig Borer, fully rebuilt and carrying maker's guarantees.

Capacity: 18in. by 12in. Table 14in. Spindle Nose to top of

NEWALL 836 Thread Grinder.

NEWALL 10-U Lapping Machine.

No. 16 BLANCHARD Surface Grinder.

All ex rebuilt stock.

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Mitchell 81 in. S.S. & S.C. Gap
Bed A.G.H. Lathe with 3in. Hollow
Spindle. Speed range 30-400 r.p.m. Further
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C. & G. OLDFIELD, Ltd. 15, Abercorn Street, PAISLEY. Member of B.A.M.T.M.

DOUGLAS

OF HIGH WYCOMBE

SECONDHAND MACHINES

FOR

IMMEDIATE DELIVERY

LATHES AND CAPSTANS

CHALLENGER S & S.C., 5in. Centre Lathe. HERBERT SMALLPIECE No. 9WSL Multicut Production Lathe. £345 LANG 7in, High Speed Finishing Lathe. £450 MYFORD DRUMMOND 3\frac{1}{2}in. Centre

SMART & BROWN 4in. Centre Lathe. £110 SOUTHBEND S.S. & S.C. 4fin. Centre Lathe.

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HERBERT in. cap. High Speed Bench Drill FOLDING AND BENDING

COBURN 6ft. × 18 gauge Folding Machine BESCO 31ft. × 18 gauge Folding Machine.

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ABWOOD Surface Grinding Machine (hand feeds), Model TH2AP. £375
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JONES & SHIPMAN Universal Cylindrical Grinder, Model 1027. £750

MILLING MACHINES BEAVER Model A Turret Mill, 28in. X

PARKSON 2P Horizontal, 52in. X

PRESSES

HILMOR Tube Bending Machine.

AUTOMATICS BULLARD Multi-Au-Matic 7in. 8 spindle. BULLARD Multi-Au-Matic 12in. 6 spindle.

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KEARNS Model OB Horizontal Boring and
Facing Machine, 2½in. diameter travelling
spindle (1957).

UNION Model BFT100 Horizontal Boring and
Facing Machine, 4in. diameter travelling
spindle (1955).

KEARNS Model Ober Stribental Boring Machine,

KEARNS Model OC Horizontal Boring Machine, 3in. dia, travelling spindle.
KEARNS No. 4 Horizontal Boring and Facing Machine, 4in. diameter travelling spindle.
WEBSTER & BENNETT Vertical Boring Machine, table 50in. diameter.
RICHARDS Type PRT Horizontal Floor Boring Machine, 34in. travelling spindle, 28in. diameter facing head.

CAPSTAN AND CENTRE LATHES CHURCHILL-REDMAN Model 13NM Heavy-Duty S.S. & S.C. Gap Bed Centre Lathe, 13in, centre height × 72in, between centres.

13in. centre height × 72in. between centres. Swing in gap 50in.
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OLDFIELD & SCHOFFIELD Surfacing and Boring Lathe, 10in. centre height.
WARD 78 Combination Turret Lathe.
NILES Heavy Duty Centre Lathe, S.S. & S.C.,
NILES Heavy Duty Centre Lathe, s.S. & S.C.,
U.L.S.O. Have Control Centre over centres.
U.L.S.O. the Control Centre Centre Centre Centre 16in. centre height × 30ft, between centres.

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ORCUTT Model HM24 Hydraulic Internal Gear Grinder. GLEASON 3in. Straight Bevel Gear Generator.

GRINDING MACHINES CRAVEN Roll Grinding Machine, capacity 20in. swing × 138in. between centres.
CHURCHILL Model HBY Internal Grinding

CHURCHILL Plain Cylindrical Grinding Machine, 26in. swing × 84in. between centres (1951)

LANDIS Type C Plain Hydraulic Cylindrical Grinding Machine, 6in. swing × 18in, between

centres.

ORCUTT Model HM24 Internal Spur Gear

Grinding Machines,
CHURCHILL Plain Hydraulic Cylindrical
Grinding Machine, 20in. swing × 72in. between centres.

BROWN & SHARPE Plain Cylindrical Grinding Machine, 10in, swing × 36in, between centres.

MILLING MACHINES

CINCINNATI Model 5/72 Plain Hydromatic Milling Machine, table 91in. × 22in. (1952). CINCINNATI No. 2L Plain Horizontal Milling Machine, table 52in. × 10in.
CINCINNATI No. 1M Vertical Milling Machine, CINCINNATI No. 4 Dial Type Horizontal Willing Machine.

Milling Machine.

PRAIT & WHITNEY Model BL3620 3-spindle
"Keller" Die Sinking Machine.

GENTEG Model 3R Automatic Production
Milling Machine, table 25in. × 16in.

MISCELLANEOUS LANGE & GAILEN 28in. stroke Double Headed Hydraulic Shaping Machine

TAYLOR & CHALLEN Double Sided 50-ton

Geared Power Press, 10in. stroke.

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LONDON, E.C.1.

Tel. CLE. 6064 & 3602.

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JONES & SHIPMAN 10in. × 27in. Universal

LATFIES

RIVET Instrument Lathe, 4 in. × 24in.

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A KERSHAW Vert, Mill 18in. × 7in.
RIGHMOND 0.1 Horizontal 30in. × 8in.
CENTEO No. 8R Auto-cycle, pro mill.
HEY Duplex Spline Mill. £175.
ADGOOK & SHILPEY IVM Vert. 25in × 7in.

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MISCELLANEOUS

MISCELLANEOUS
BOTNIA 5ft. × 18in. Planer.
RAPIDOR 8in. × 8in. heavy duty power saw.
MANURHIN TRI2-16 fin. Auto. 1958.
T.T. & H. Engraver CB with div. table.
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THIEL Filing and Sawing Machine. 295.
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THIEL Punch Shaper. THIEL Punch Shaper.
ORMEROD 12in. Shaper with Cam Cutting

Other machines in stock.

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WE SELL

Lang 20in. Surfacing and Boring Lathe, Chuck Model. Excellent Machine.

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A squith type H.D.P. two-spindle Profile Milling M/c. Adjustable cross-rail. Ind. motor drive to each spindle. Capacity 24in. × 28in. Spindle speeds 250-3,000 r.p.m.—LEE & HUNT LTD., Crocus Street, Nottingham. Thone 84246.

HERBERT 11in. Pedestal Drill. CORONA 4ft. Radial Drill. £825.

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HERBERT HUNT Tap and Reamer. £65.
SCRIVENER No. 1 Centreless, with auto feed.
SMART & BROWN Internal Grinder. 1 in. Max. NORTON 18in. × 7in. Hyd. Cyl. Grinder. £395.

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MURAD fin. 82 Capetan, full equip.
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BLISS 250 ton Coining Press,
BLISS 21B 60 ton geared. Adj. Str.
BLISS 21B 60 ton geared. Adj. Str.
BLISS 20B 20 ton Roll feed. Adj. Str.
BLISS 20B 20 ton Roll feed. Adj. Str.
BLISS 20 20 ton.
WARD 20 ton.
WARD 20 ton.
TAYLOR & GHALLEN 10 ton.
SEDGWICK 12ft. × †in. Folder.
BESGO 10 ton Power Press. £175.
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BEAVER Model A Turret 17111, 40111.

table. (As New.)

CINCINNATI No. 3 Sliding Head

Dial Selection, 63 in. × 15in. table.

2750

CINCINNATI No. 3 Sliding Head

Vertical.

55in. × 134 in. table.

DENBIGH C4 Universal Mill, 46in. × 10in.

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£85

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BUTLER Planer, 9ft. × 2\ft. table.

EHRENFELD Planing Machine, 13ft. × 3\ft. table.

£1,400

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Teaded 50-ton

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machine tools for BELLS .

capacity. Inclinable, ungeared, open fron Fixed stroke 3in. Bed 274in. by 18in. to guides 124in. M.D. 400/3/50.

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PRECIMAX Hydraulic Vertical Spindle Surface Grinder. Segmental wheel 18in. dia. Grinding cap. 16in. by 48in. M.D. 400/3/50.

NORTON 48in. by 12in. Horizontal Hydraulic Surface Grinder. Admits 17in. under wheel. Grinding wheel size 12in. by 21in. max. Hydraulic table and cross feed to head. With 12in. by 48in. chuck and 400/3/50

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H. BELL (Machine Tools) LTD., Walter Street, LEEDS 4.

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British Federal 50 kVA Flash Butt Welding Machine. 400/3/50.
Fielding 50 ton hydraulic horizontal pipe bender, up to 6in, bore hydraulic tubes. 200 Ton Fielding Downstroke Hydraulic Press, 14in ram, 42in. stroke, 63in, daylight. 100 Ton Fielding ditto. 10in. ram, 72in. stroke, 95in, daylight. 50 Ton Fielding ditto. 3ft. stroke.

Bliss 70 Ton Geared Double Sided Power Stroke, 99in, 45in, 50 Ton Geared Double Sided Power Stroke, 98in, 50 Ton Geared Double Sided Power Stroke, 98ins, 50 tons. American. Bennie Punching, Shearing and Section Cropping Machine, 48in. × 44in. × 4in. angle. Windsor 6-os. Plastic Injection Moulding Machine.

Windsor 6-os. Plastic Injection Moulding Machine.
Sedgewick Bending and Folding Machine.
6ft. × \$in., motorised.
8ft, × \$in. Bennie Bending Rolls.
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200 Tons Tangve Hydraulic Straightening Press, bed 25ft. × 3ft., stroke 21ln., motorised travelling table, 2 ram pump.
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Pels Punch Shears and Cropper, 12in. blade, shear şin. takes 6in. × 6in. × \$in. angles.
Robertson Shears, *in. capacity, 10 h.p.
28in. blade, 9in. maximum opening. (Iwo.)
Berry Plate Gulliothe, capacity, 10 h.p.
10 Ton Harball Fleming, 29ft. span, cab control.
25 Ton Clyde, 21ft. 9in. span, cab control.

25 Ton Clyde, 21ft. 9in. span, cab control 1954. Can convert any span to 95ft. 20 Ton Vaughan 42ft. 3in. span. Unused. 20 Ton Morris Goliath, 35ft. span, 5 ton auxiliary.

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10 Toh, 60ft, span. 1955, (Two.)
5 Ton, 37ft. span. 1944.
3 Ton Morris, 149ft. span. 1954.

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PRECIMAX Cylindrical Plain Grinder. Capacity Sin. 24in. Plunge feed. Coolant tank and fittings. 400/3/50.

ARCHDALE 28in. All Purpose Horizontal Milling Machine. Table size 38in. × 13in. Power and Rapid Power traverse 100/3/50. Spindle speeds 30 to 462 rp. m.

all ways. Spindle speeds 30 to 462 r.p.m. 400/3/50.

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SWEENNEY & BLOCKSIDGE NO. 9 Geared, Inclinable, Power Press, Pressure 20 tons. Adjustable stroke 1in. to 4in. Motorised 400/3/50. Operator's Guards. H.M.E. Type L40 Ungeared, Open Front, Inclinable, Power Press, Pressure 40 tons. Adjustable Stroke 4in. to 4in. Bed area 294in. × 214in. 400/3/50. Operator's

29 in. × 21 in. 400/3/50. Operator's Guards.

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RUSHWORTH Geared, Overcrank, Power Guillotine. Capacity 10ft. × in. m.s. 20 strokes per minute. Motorised 15 h.p., 400/3/50. Complete with automatic hold-down, front and rear guards, fully guarded and spare set of blades.

BROOKES Overcrank, Double Geared, Power Guillotine, capacity 4ft. × in. Powered Work table in two sections) 24ft. long approx. × 4ft. wide. 20 h.p., 400/3/50.

400/3/50.

RHODES No. 12 Double Sided, Double Crank, Geared, Power Press. Pressure 70 tons. Fitted fixed stroke 4in. Bed area 44in. × 42in. 400/3/50.

STANCROFT LTD., LANCASTER STREET, BIRMINGHAM, 4.

ASTon Cross 2235.



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MILLING MACHINES
MILWAUKEE 2K Universal.
DENBIGH 40 Universal.
DENBIGH 40 Universal.
RICHMOND 0.1 Universal.
ARCHDALE 28in. Production.
CINCINNAT 1-12 Production.
P. & W. Slab Mill Prod.
CINCINNAT No. 2 Vert.
HERBERT 158 Vert.
HERBERT 18V Vert.
ASQUITH Profile Mill. £1.250. £325. £250. £350. £350. £155. £1.450. £525. £595. £450.

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J. & S. Tool and Cutter.
WICKMAN Auto Cutter.
HUNT No. 2 Drill.
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ARTER 12In. Ring.
B. & S. No. 13 Universal.
No. 13 Universal.
ARTER 12In. by 24in. Uni.
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NOVAMATIC Type B Internal £275 £225. £235. £495. £750. DRILLING MACHINES

K. & W. 4ft. Heavy Radial. CINCINNATI 4 Morse. BAUGH Radial Tapper.

THE CAUSEWAY, EGHAM SURREY

EGHAM 4166-7

MACHINES NOW IN STOCK

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MATHEYS Model FPN/28 Semi Jig

PADDON MK3 type WP Cylinder Re-boring Machines.

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BOLEY-LEINEN Model ERIS Jin. Capstan (modern).

HERBERT No. 2 Pre-optive Bar Turret Lathe, Flamard bed, 2in. capacity with bar feed, full turret tooling.

HERBERT Model 22A Turret Lathe. 84in. S.P. Hole.

LIBBY 2H 8in. spindle Turret Lathe.

CENTRE LATHES

SOUTHBEND 7in, Centre Lathe.

CRAVEN Heavy Duty Railway Wheel Lathe, swing 6ft. × 12ft. vee belt drive. Weight 25 tons.

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VICO (Swiss) Hydraulic Toolroom Universal Grinder 10in, by 30in.

LAMBERT Model 73 Watchmaker's Cutter Grinders (two).

CRAVEN Heavy Duty Roll Grinding Machine with capacity for rolls 42in. dia. by 12ft. between centres and fitted with automatic cambering. Will take rolls up to 25 tons weight. Fully motorised machine of modern design. WEIGHT 25 tons.

WALDRICH SIEGEN Roll Grinder. 36in. by 13ft. between centres.

Two CINCINNATI No. 2 Tool and Cutter Grinding Machines.

COVEL No. 2 Tool and Cutter Grind-

IMPERIA Tool and Cutter Grinder, Model M6 AR.

MATRIX No. 16G Plain Straight Thread

MATRIX No. 6 Internal Thread Grinders, 3in. by 10in.

HEALD Model 81 Sizematic Internal Grinder

WOLTERS Model I.L.I Hydraulic Internal Lapping Machine.

PETEWE Model 3D Profile Grinding Machine. (Nearly new.)

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VICTORIA Duplomatic Hydraulic Copy Milling Machine, 8in. by 8in. (NEW).

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PACERA in. Bench Drill (New).

Two ARCHDALE 36in. Radial Drilling Machines. No. 4 M.T. CRAFTSMAN in. Bench Drills; four

Various ACIERA Precision Bench Drills.

GUILLOTINES

BESCO 42in. by 10 s.w.g. Power Guillotine.

HANDS 4ft. by in. Guillotine.

RHODES 6ft. by in. Guillotine.

MILLING MACHINES

EDGWICK No. 1 Horizontal Milling Machine 40in, by 10in, table.

DENBIGH Model No. C4 Horizontal Milling Machines.

SANT ANDREA Model U.F.O/5 Extra heavy duty Horizontal Miller. 864in. by 19in. Table travel 67in.

VICTORIA Junior Omnimil (New). Two ARCHDALE 18in. Automatic Cycle Kneeless Production Millers.

VICTORIA Model V2 Vertical Mill (Nearly new).

CUNLIFFE & CROOM No. 2 Vertical Mill (dial). ARCHDALE 34in. Plain Horizontal Miller (nearly new).

PLANING MACHINES

STIRK 16ft. by 5ft. by 5ft. double column Planers. four toolboxes; modern Planers, four toolboxes; modern machines with Lancashire drive (Two).

. . . a few yards from Olympia and Earls Court

POWER PRESSES RHODES 3-ton Open Fronted Bench Press with flange motor and UDAL

guards.

LEE& CRABTREE 15-ton Horning Press.

LEE& CRABTREE 20-ton Horning Press.

LEE & CRABTREE 35 Double Action chanical Press

Mechanical Press.

Model AMP

22-ton Power Presses.

Mechanical Press.

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SHAPING MACHINES

BERRY 16in. Shaper.
BROOK 18in. Shaping Machine.
KLOPP 22in. Shaping Machine.
TORPEX 22in. Shaping Machine.

SAWING AND FILING MACHINES

WESPA AS4 Bandsawing and Bandfiling Machine, hydraulic feed (similar Do-all V/16).

WATCHMAKERS' MACHINES

MIKRON No. 79 Gear Hobber (almost new). SAFAG Model 24 Cutter Relieving LAMBERT Model 66 Gear Hobber.

MACHINES JUST BOUGHT FOR STOCK

MILWAUKEE Model 5H Vertical Mill, MILWAUKEE Model SH Vertical Mill, dial type, high speed model with power down feed to head, table 94in. × 18in. (New Price U.S.93.680. This machine is in beautiful condition, offered at a fraction of replacement cost.)

ASQUITH Model ID1 4ft. Radial.

OLIVETTI Model R 4-500 plain cylindrical grinder (1953).

MOPCO Model RUP(108YW. Combination, horizontal and vertical spindle

HOPCO Model RUP108YW. Combina-tion, horizontal and vertical spindle toolroom hydraulic Surface Grinder, table 38in. x 1 lin. (1953). ZENITH Model PH Horizontal Spindle Hydraulic, Surface Grinder, 24in. x 8in. (1953). SOMUA Model SH2C Horizontal Miller, rable 67in. x 14ii. (1953).

table 67in. × 14in. (1953).

IMPERIA Model MR26 Tool and Cutter

Grinder (1953).
HERBERT Model 22A Turret Lathe, spindle hole 8½in., weight 12 ton.
CUNCLIFFE & CROOM No. 2 Vertical

Mill (dial).
VICTORIA Model V2 Vertical Mill

(1956). ARCHDALE 34in. Dial type Horizontal Mill, table 63in. by 15in. (1953).
FACEPLATE LATHE, 9ft. swing.
RYDERMATIC No. 18 vertical Auto-

matic Heavy VICO (Swiss Built) Model 750 Hydraulic Universal Toolroom Grinder, 10in. × 30in. (1953).



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RHODES 6ft. × 14 gauge Power Bending

CROPPING MACHINES

Double Ended Angle Cropping Machine. Cap. up to 6in. × 1in. angles.

DRILLING MACHINES

POLLARD 13in. Pillar Drill, No. 2 Morse Taper. R. & F. Table 11in. × 11in. AMERICAN 6ft. H/Duty Radial Drill, No. 6 M.T. Older machine, in good condition. 400/3/50. Sep. motor.

FOLDING MACHINES

EDWARDS 6ft. × 1 in. High Lift Swing Beam Universal Folder.

GRINDING MACHINES

New NORTON 10in., 12in., 14in., 16in. and 20in. D/E Tool Grinders.

ABRASIVE No. 34 24in. × 8in. Vertical Spindle Surface Grinder.

GUILLOTINES

KEYSEATING MACHINES

EDGWICK Keyseater. Stroke 41in. Table

LATHES

HERBERT No. 4 Capstan. 21in. H/Spindle. Speeds 511.

MILLING MACHINES

EDGWICK No. 2 Horizontal Miller. Table 46in. × 11in.
MILWAUKEE 3H Vertical Milling Machine,

NIBBLERS

BURFREE 2A Nibbling Machine, Cap. in. M/S. W.F. 14 Gauge Nibbler. 59in. throat.

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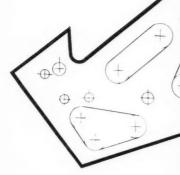
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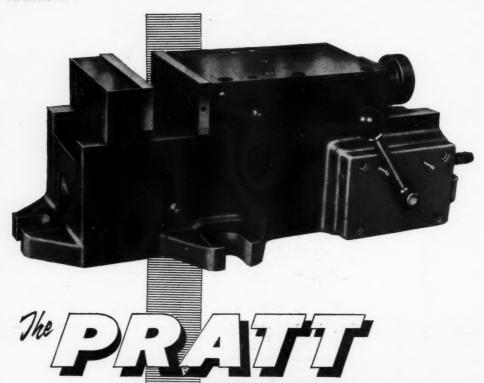
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